# **Power System Analysis**

#### **Chapter 5 Branch flow models: radial networks**

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# **Outline**

- 1. Radial networks
- 2. Equivalence
- 3. Backward forward sweep
- 4. Linear power flow model

# **Outline**

- 1. Radial network
	- Line model
	- With shunt admittances
	- Without shunt admittances
	- Power flow solution
- 2. Equivalence
- 3. Backward forward sweep
- 4. Linear power flow model

# **Line model** 0

- 1. Network  $G:=(N,E)$ can be obtained from *Y* through Kron reduction making use of the fact that the internal injection *I*<sup>3</sup> = 0;
	- $\overline{N}:=\{0\}\cup N:=\{0\}\cup\{1,...,N\}$  : buses/nodes/terminals
- $E \subseteq \overline{N} \times \overline{N}$  : lines/branches/links/edges  $L \subseteq I$
- 2. Each line  $(j, k)$  is parameterized by  $\left(\right. \mathbf{y}_{jk}^s, \mathbf{y}_{jk}^m \right)$  and  $\left(\right. \mathbf{y}_{kj}^s, \mathbf{y}_{kj}^m \right)$  $\binom{C}{K}$   $\binom{C}{K}$   $\binom{C}{K}$   $\binom{C}{K}$   $\binom{C}{K}$
- $(y_{jk}^s, y_{jk}^m)$  : series and shunt admittances from  $j$  to  $k$
- $(y_{kj}^s, y_{kj}^m)$  : series and shunt admittances from  $k$  to  $j$
- Models transmission or distribution lines, single-phase transformers



#### **Line** model the state  $\mathbf{L}$ represent a transmission or distribution line or transformer. We also write *j* ⇠ *k* instead of (*j, k*) 2 *E*. We

$$
I_j, s_j \xrightarrow{V_j} I_{jk}, S_{jk} \qquad S_{kj}, Y_{kj} \qquad S_{kj}, I_{kj} \qquad (k \qquad s_k, I_k
$$

Sending-end currents

 $I_{jk} = y_{jk}^{s}(V_j - V_k) + y_{jk}^{m}V_j, \qquad I_{kj} = y_{kj}^{s}(V_k - V_j) + y_{kj}^{m}V_k,$ is also a per-phase model of balanced three-phase lines. A line has two terminals (*j, k*) and is specified  $\partial f(x) = \int_{jk}^{m} V_j$ ,  $I_{kj} = y_{kj}^{s}(V_k - V_j) + y_{kj}^{m} V_k$ , admittance of the line at terminal *j*, and *y<sup>m</sup> k j* is the shunt admittance of the line at terminal *k*; see Figure 4.1.

If  $y_{jk}^s = y_{kj}^s$ : same relation but equivalent to  $\Pi$  circuit:  $V_j$  is the integral of  $V_k$  is the  $V_k$ If  $y_{jk}^s = y_{kj}^s$ : same relation but equivalent to  $\Pi$  circuit:



#### **Line** model the state  $\mathbf{L}$ represent a transmission or distribution line or transformer. We also write *j* ⇠ *k* instead of (*j, k*) 2 *E*. We

$$
I_j, s_j \rightarrow \underbrace{\begin{pmatrix} V_j & I_{jk}, S_{jk} & S_{kj}, I_{kj} & V_k \\ \hline \end{pmatrix}}_{\textcolor{red}{\big(\begin{pmatrix} y_{jk}^s, y_{jk}^m \end{pmatrix}, \begin{pmatrix} y_{kj}^s, y_{kj}^m \end{pmatrix}}}, \underbrace{S_{kj}, I_{kj}}_{\textcolor{red}{\big(\begin{pmatrix} k \\ k \end{pmatrix}} \leftarrow s_k, I_k}
$$

Sending-end currents

$$
I_{jk} = y_{jk}^{s}(V_j - V_k) + y_{jk}^{m} V_j, \qquad I_{kj} = y_{kj}^{s}(V_k - V_j) + y_{kj}^{m} V_k,
$$

Recall: bus injection models relate nodal variables  $(s,\,V)$  and are suitable for general networks

$$
s_{j} = \sum_{k:j \sim k} \left( y_{jk}^{s} \right)^{H} \left( |V_{j}|^{2} - V_{j}V_{k}^{H} \right) + \left( y_{jj}^{m} \right)^{H} |V_{j}|^{2}
$$

#### **Line** model the state  $\mathbf{L}$ represent a transmission or distribution line or transformer. We also write *j* ⇠ *k* instead of (*j, k*) 2 *E*. We

$$
I_j, s_j \longrightarrow \overbrace{\left(j\right)}^{V_j} \xrightarrow{I_{jk}, S_{jk}} \qquad \qquad S_{kj}, I_{kj} \xrightarrow{V_k} \qquad \qquad S_{kj}, I_{kj} \qquad \qquad (y_{jk}^s, y_{jk}^m), (y_{kj}^s, y_{kj}^m) \qquad \qquad (k \longmapsto s_k, I_k
$$

Sending-end currents

$$
I_{jk} = y_{jk}^{s}(V_j - V_k) + y_{jk}^{m}V_j, \qquad I_{kj} = y_{kj}^{s}(V_k - V_j) + y_{kj}^{m}V_k,
$$

Branch flow models: key features

- . Key reatures<br>variables.gs.well • Involve branch variables as well
- Particularly suitable for distribution systems which are mostly radial networks
- Variables contain no voltage/current phase angles (only magnitudes)<br>• Can recover voltage/current angles due to tree topology
	- Can recover voltage/current angles due to tree topology
- Carriecover voltage/current angles due to tree topology<br>• Equivalent to bus injection model Liquivalent to bas injection model

## **Radial network With shunt admittances: variables**

For each bus *j*

- $s_j := (p_j, q_j)$  or  $s_j := p_j + iq_j$ : power injection
- $v_j$ : squared voltage magnitude

For each branch  $(j,k)$ 

- $\left(\,\mathscr{C}_{ik},\mathscr{C}_{ki}\,\right)$  : squared magnitude of sending-end current  $j\rightarrow k$ , and  $\left(\ell_{jk},\ell_{kj}\right)$  : squared magnitude of sending-end current  $j\rightarrow k,$  and  $k\rightarrow j$
- $S_{ik}:=\big(\,P_{ik},Q_{ik}\,\big)$  or  $\,S_{ik}:=P_{ik}+iQ_{ik}$  : sending-end power  $j\to k;$  also  $S_{ki}$  from  $S_{jk} := \left(\, P_{jk}, Q_{jk}\,\right) \,$  or  $\,S_{jk} := P_{jk} + i Q_{jk}$  : sending-end power  $j \to k$ ; also  $S_{kj}$  from  $k \to j$

The variables  $v_j$  and  $\left(\,\mathscr{C}_{jk},\mathscr{C}_{kj}\,\right)$  contain no angle information Angles must be recovered from a power flow solution  $x := (s, v, \ell, S) \in \mathbb{R}^{3(N+1)+6M}$ 

• This is easy for radial networks; trickier for meshed networks

For each line  $(j, k)$  let:

 $\alpha_{jk} = \alpha_{kj}$  if and only if  $y_{jk}^m = y_{kj}^m$  $\alpha_{jk} := 1 + z_{jk}^s y_{jk}^m$ ,  $\alpha_{kj} := 1 + z_{kj}^s y_{kj}^m$ 

 $\alpha_{jk} = \alpha_{kj} = 1$  if and only if  $y_{jk}^m = y_{kj}^m = 0$ 

$$
z_{jk}^s := \left(y_{jk}^s\right)^{-1}, \quad z_{kj}^s := \left(y_{kj}^s\right)^{-1}
$$

# **Radial network**

#### **With shunt admittances**

$$
s_j = \sum_{k:j \sim k} S_{jk}
$$

power balance

# **Radial network**

**With shunt admittances**

$$
s_j = \sum_{k:j \sim k} S_{jk}
$$
  

$$
\left| S_{jk} \right|^2 = v_j \mathcal{C}_{jk}, \qquad \left| S_{kj} \right|^2 = v_k \mathcal{C}_{kj}
$$

power balance

branch power magnitude

The complex notation is only shorthand for real equations  $\mathbf{v} = \sum_{n} p_n$   $\mathbf{z} = \sum_{n} p_n$ *αjk vj* − (*z<sup>s</sup>*  $v_i \mathcal{C}_{ik} = P_{ik}^2 + Q_{ik}^2, \qquad v_k \mathcal{C}_{ki} =$  $p_j = \sum$ *k*  $P_{jk}$ ,  $q_j = \sum_j$ *k Qjk*  $v_j \mathcal{C}_{jk} = P_{jk}^2 + Q_{jk}^2, \qquad v_k \mathcal{C}_{kj} = P_{kj}^2 + Q_{kj}^2$ 

 $s_j = \sum S_{jk}$ *k*:*j*∼*k Sjk* 2  $= v_j \ell_{jk}$ ,  $|S_{kj}|$ 2  $= v_k \ell_{kj}$ *αjk* 2  $v_j - v_k = 2$  Re  $\left( \alpha_{jk} \left( z_{jk}^s \right)$   $S_{jk} \right) - \left| z_{jk}^s \right|$ 2  $\ell_{jk}$ *αkj* 2  $v_k - v_j = 2$  Re  $\left( \alpha_{kj} \left( z_{kj}^s \right)$   $S_{kj} \right)$  −  $\left| z_{kj}^s \right|$ 2  $\ell_{kj}$ 

power balance

branch power magnitude

Ohm's law, KCL (magnitude)

 $s_j = \sum S_{jk}$ *k*:*j*∼*k Sjk* 2  $= v_j \ell_{jk}$ ,  $|S_{kj}|$ 2  $= v_k \ell_{kj}$ *αjk* 2  $v_j - v_k = 2$  Re  $\left( \alpha_{jk} \left( z_{jk}^s \right)$   $S_{jk} \right) - \left| z_{jk}^s \right|$ 2  $\ell_{jk}$ *αkj* 2  $v_k - v_j = 2$  Re  $\left( \alpha_{kj} \left( z_{kj}^s \right)$   $S_{kj} \right)$  −  $\left| z_{kj}^s \right|$ 2  $\ell_{kj}$  $\alpha_{jk}^{\text{H}} v_j - \left(z_{jk}^s\right)$   $S_{jk} = \left(a_{kj}^{\text{H}} v_k - \left(z_{kj}^s\right)$   $S_{kj}\right)$ power balance branch power magnitude Ohm's law, KCL (magnitude) cycle condition:  $V_j \overline{V}_k = (V_k \overline{V}_j)$ 

 $2(N + 1) + 6M$  real equations in  $3(N + 1) + 6M$  real vars  $x := (s, v, \ell, S) \in \mathbb{R}^{3(N+1)+6M}$ 

 $s_j = \sum S_{jk}$ *k*:*j*∼*k Sjk* 2  $= v_j \ell_{jk}$ ,  $|S_{kj}|$ 2  $= v_k \ell_{kj}$ *αjk* 2  $v_j - v_k = 2$  Re  $\left( \alpha_{jk} \left( z_{jk}^s \right)$   $S_{jk} \right) - \left| z_{jk}^s \right|$ 2  $\ell_{jk}$ *αkj* 2  $v_k - v_j = 2$  Re  $\left( \alpha_{kj} \left( z_{kj}^s \right)$   $S_{kj} \right)$  −  $\left| z_{kj}^s \right|$ 2  $\ell_{kj}$  $\alpha_{jk}^{\text{H}} v_j - \left(z_{jk}^s\right)$   $S_{jk} = \left(a_{kj}^{\text{H}} v_k - \left(z_{kj}^s\right)$   $S_{kj}\right)$ power balance branch power magnitude Ohm's law, KCL (magnitude) cycle condition:  $V_j \overline{V}_k = (V_k \overline{V}_j)$ 

Any  $x := (s, v, \ell, S) \in \mathbb{R}^{3(N+1)+6M}$  that satisfies these equations with  $(v, \ell) \geq 0$  is a **power flow solution** 

All equations are linear in  $x$ , except the quadratic equalities

$$
\left| S_{jk} \right|^2 = v_j \mathcal{C}_{jk}, \quad \left| S_{kj} \right|^2 = v_k \mathcal{C}_{kj}
$$

There may be 0, 1, or  $>1$  power flow solutions

This can be relaxed to second-order cone constraint in OPF (later)

#### **Example 2-bus network**

Buses  $j$  and  $k$  connected by a transformer characterized by  $(K, \tilde{y}^s, \tilde{y}^m)$  (voltage gain  $K$  may be complex) Line parameters are:

$$
y_{jk}^s := \frac{\tilde{y}^s}{K}, \quad y_{jk}^m := \left(1 - \frac{1}{K}\right) \tilde{y}^s, \quad y_{kj}^s := \frac{\tilde{y}^s}{\bar{K}} \quad y_{kj}^m := \frac{1}{|K|^2} \left( (1 - K)\tilde{y}^s + \tilde{y}^m \right)
$$

BFM:

$$
v_j - v_k / |K|^2 = 2 \operatorname{Re} \left( \left( \tilde{z}^s \right)^{H} s_j \right) - | \tilde{z}^s |^2 \mathcal{C}_{jk} \qquad \qquad \tilde{z}^s := (\tilde{y}^s)^{-1}
$$
  
\n
$$
|\tilde{\alpha}/K|^2 v_k - v_j = 2 \operatorname{Re} \left( \tilde{\alpha} \left( \tilde{z}^s \right)^{H} s_k \right) - | K \tilde{z}^s |^2 \mathcal{C}_{kj}
$$
  
\n
$$
\left| s_j \right|^2 = v_j \mathcal{C}_{jk}, \qquad \left| s_k \right|^2 = v_k \mathcal{C}_{kj}
$$
  
\n
$$
v_j - (\tilde{z}^s)^{H} s_j = (\tilde{\alpha}/|K|^2) v_k - \tilde{z}^s \bar{s}_k
$$

**Assume:**  $y_{jk}^s = y_{kj}^s$  and  $y_{jk}^m = y_{kj}^m = 0$ 

Then

1. 
$$
\alpha_{jk} = \alpha_{kj} = 1
$$
  
2.  $\ell_{kj} = \ell_{jk}$  and  $S_{kj} + S_{jk} = z_{jk}^s \ell_{jk}$ 

Can use directed graph with vars  $\ell_{ik}, S_{ik}$  defined only in direction of lines Substitute  $\ell(\mathscr{C}_{ki},S_{ki})$  in terms of  $\ell(i_k,S_{ik})$  into previous power flow equations yields original DistFlow equations of [Baran-Wu 1989]  $\left(\ell_{jk},S_{jk}\right)$  defined only in direction of lines  $j\rightarrow k\in E$  $\left(\ell_{kj}, S_{kj}\right)$  in terms of  $\left(\ell_{jk}, S_{jk}\right)$ 

DistFlow equations [Baran-Wu 1989]:

$$
\sum_{k:j\to k} S_{jk} = \sum_{i:i\to j} \left( S_{ij} - z_{ij}^s \mathcal{C}_{ij} \right) + s_j
$$
  

$$
v_j - v_k = 2 \operatorname{Re} \left( z_{jk}^s \mathbf{S}_{jk} \right) - |z_{jk}^s|^2 \mathcal{C}_{jk}
$$
  

$$
v_j \mathcal{C}_{jk} = |S_{jk}|^2
$$

power balance Ohm's law (magnitude) branch power magnitude 0

*i*

*j*

*k*

- Cycle condition becomes vacuous (because  $S_{kj} := z_{jk}^s \mathcal{C}_{jk} S_{jk}$ )
- $2(N + 1) + 2M$  real equations in  $3(N + 1) + 3M$  real vars
- e.g. given  $(v_0,s_j,j\in N)$ , there are  $4N+2$  equations in  $4N+2$  vars  $(s_0,v_j,j\in N,\ell,S)$

All equations are linear in  $x$ , except the quadratic equalities

$$
v_j \mathcal{C}_j = \left| S_{jk} \right|^2
$$

There may be 0, 1, or  $>1$  power flow solutions

This can be relaxed to second-order cone constraint in OPF (later)

## **Angle recovery**

Given power flow solution  $x := (s, v, \ell, S)$ , define nonlinear functions

$$
\beta_{jk}(x) := \angle \left(\alpha_{jk}^H v_j - \left(z_{jk}^s\right)^H S_{jk}\right)
$$
  

$$
\beta_{kj}(x) := \angle \left(\alpha_{kj}^H v_k - \left(z_{jk}^s\right)^H S_{kj}\right)
$$

 $C$ ycle condition ensures that  $(\beta_{jk}(x), \beta_{kj}(x))$  are angle differences across line  $(j, k)$ , i.e.,

 $\exists$  voltage angles  $\theta$  s.t.  $\beta(x) = C^{\mathsf{T}} \theta$ 

#### **Angle recovery:**

1. Tree topology  $\implies \theta = C(C^{\dagger}C)$ −1  $\beta(x) + \phi$ **1** 

2.  $V_j := \sqrt{v_j} e^{i\theta_j}$ ,  $I_{jk} := \sqrt{\ell_{jk}} e^{i(\theta_j - \angle S_{jk})}$ 

### **Summary BFM for radial network**

$$
s_{j} = \sum_{k:j\sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| \alpha_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^{s} \right)^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{s} \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
\left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{s} \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
\alpha_{jk}^{\mathsf{H}} v_{j} - \left( z_{jk}^{s} \right)^{\mathsf{H}} S_{jk} = \left( \alpha_{kj}^{\mathsf{H}} v_{k} - \left( z_{kj}^{s} \right)^{\mathsf{H}} S_{kj} \right)^{\mathsf{H}}
$$
\n
$$
\left| \alpha_{jk}^{\mathsf{H}} v_{j} - \left( z_{jk}^{s} \right)^{\mathsf{H}} S_{jk} = \left( \alpha_{kj}^{\mathsf{H}} v_{k} - \left( z_{kj}^{s} \right)^{\mathsf{H}} S_{kj} \right)^{\mathsf{H}}
$$
\n
$$
\text{Distribow}
$$
\n
$$
BFM\text{-}radial
$$

### **Example: power flow solution 2-bus network**

Two buses 0 and 1 connected by a line with series impedance  $z = r + ix$  (graph orientation: up)

$$
p_0 - r\ell = -p_1, \quad q_0 - x\ell = -q_1
$$
  

$$
v_1 - v_0 = 2 (rp_1 + xq_1) - (r^2 + x^2)\ell
$$
  

$$
p_1^2 + q_1^2 = v_1\ell
$$

Given:  $r = x = 1$  and  $v_0 = 1$ ,  $q_1 = 0$ , find  $(p_0, q_0, v_1, \ell)$  and show that  $(v_1(p_1), p_1)$  forms an ellipse

#### **Solution**

Eliminate 
$$
v_1 \Rightarrow 2e^2 - (1 + 2p_1)e + p_1^2 = 0
$$
. Hence  $(\Delta := 4p_1(1 - p_1) + 1)$   
\n
$$
e = \frac{1}{4} \left( 1 + 2p_1 \pm \sqrt{\Delta} \right), \quad p_0 = \frac{1}{4} \left( 1 - 2p_1 \pm \sqrt{\Delta} \right), \quad q_0 = \frac{1}{4} \left( 1 + 2p_1 \pm \sqrt{\Delta} \right)
$$
\n
$$
v_1 = \frac{1}{2} \left( 1 + 2p_1 \mp \sqrt{\Delta} \right)
$$

#### **Example: power flow solution 2-bus network** Since *A* 0 is positive definite, (*p*1*, v*1) traces out an ellipse. It is shown in Figure 5.3 as the high

**Solution** 

The solution 
$$
v_1 = \left(1 + 2p_1 \mp \sqrt{\Delta}\right)/2
$$
 is equivalent to:  
\n
$$
[p_1 \quad v_1] \begin{bmatrix} 8 & -4 \\ -4 & 4 \end{bmatrix} \begin{bmatrix} p_1 \\ v_1 \end{bmatrix} - 2 \underbrace{[0 \quad 2]}_{c^T} \begin{bmatrix} p_1 \\ v_1 \end{bmatrix} + 1 = 1
$$

Points  $x \in \mathbb{R}^n$  satisfying

$$
(x - c)^T A (x - c) = x^T A x - 2c^T x + ||c||^2 = 1
$$

form an ellipse if  $A$  is real (symmetric) and positive definite



## **Hollow solution set**

Let

$$
\mathbb{X}_{\text{df}} := \{x := (s, v, \ell, S) \in \mathbb{R}^{6N+3} : x \text{ satisfies DistFlow equations }\}
$$

#### **Theorem**

Suppose network graph  $G$  is connected. If  $\hat x$  and  $\tilde x$  are distinct solutions in  $\mathbb X_{\sf df}$  with  $\hat v_0=\tilde v_0$ , then no convex combination of  $\hat{x}$  and  $\tilde{x}$  can be in  $\mathbb{X}_{\sf df}.$  In particular,  $\mathbb{X}_{\sf df}$  is nonconvex.

# **Outline**

#### 1. Radial network

#### 2. Equivalence

- Extension to general network
- Equivalence of BFM and BIM
- 3. Backward forward sweep
- 4. Linear power flow model

## **Power flow models**

Bus injection model

$$
s_{j} = \sum_{k:j \sim k} (y_{jk}^{s})^{H} (|V_{j}|^{2} - V_{j}V_{k}^{H}) + (y_{jj}^{m})^{H} |V_{j}|^{2}
$$

Branch flow models

$$
s_{j} = \sum_{k:j\sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| \alpha_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
\alpha_{jk}^{H} v_{j} - \left( z_{jk}^{s} \right)^{H} S_{jk} = \left( \alpha_{kj}^{H} v_{k} - \left( z_{kj}^{s} \right)^{H} S_{kj} \right)^{H}
$$
\n
$$
\begin{array}{c} \text{Different vars and equations} \\ \text{Both describe Kirchhoff's and Ohm's laws} \\ \text{Are they equivalent? In what sense?} \end{array}
$$

## **Power flow models**

BIM applies to general networks BFM applies to radial networks only

To show their equivalence, we first need to extend BFM to general networks with cycles

### **General network Complex form**

Let 
$$
\tilde{y}_{jk} := y_{jk}^s + y_{jk}^m
$$
 and  $\tilde{y}_{kj} := y_{kj}^s + y_{kj}^m$ 

BFM for general network:

$$
s_j = \sum_{k:j \sim k} S_{jk},
$$
  
\n
$$
I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k, \qquad I_{kj} = \tilde{y}_{kj} V_k - y_{kj}^s V_j
$$
  
\n
$$
S_{jk} = V_j I_{jk}^H, \qquad S_{kj} = V_k I_{kj}^H
$$

Does **not** assume  $y_{jk}^s = y_{kj}^s$  nor  $y_{jk}^m = y_{kj}^m = 0$ This model looks similar to BIM complex form! • It is a bridge between BFM and BIM

## **General network Real form**

$$
s_{j} = \sum_{k:j \sim k} S_{jk}
$$
\n
$$
\left| S_{jk} \right|^{2} = v_{j} \mathcal{E}_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \mathcal{E}_{kj}
$$
\n
$$
\left| \alpha_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \mathcal{E}_{jk}
$$
\n
$$
\left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} \mathcal{E}_{kj}
$$
\n
$$
\exists \theta \in \mathbb{R}^{N+1} \text{ s.t. } \beta_{jk}(x) = \theta_{j} - \theta_{k}, \ \beta_{kj}(x) = \theta_{k} - \theta_{j}
$$

power balance

branch power magnitude

Ohm's law, KCL (magnitude)

#### cycle condition

 $2(N + 1) + 6M$  real equations in  $3(N + 1) + 6M$  real vars  $x := (s, v, \ell, S) \in \mathbb{R}^{3(N+1)+6M}$ 

## **General network Real form**

Major simplification for radial network: nonlinear cycle condition becomes linear in  $x$ 

All other equations remain the same

$$
\beta_{jk}(x) := \angle \left( \alpha_{jk}^{H} v_j - \left( z_{jk}^{s} \right)^{H} S_{jk} \right)
$$
\n
$$
\beta_{kj}(x) := \angle \left( \alpha_{kj}^{H} v_k - \left( z_{jk}^{s} \right)^{H} S_{kj} \right)
$$
\n
$$
\beta(x) = \begin{bmatrix} C^{T} \\ -C^{T} \end{bmatrix} \theta \text{ for some } \theta \in \mathbb{R}^{N+1}
$$

general network

$$
\alpha_{jk}^H v_j - \left(z_{jk}^s\right)^H S_{jk} = \left(\alpha_{kj}^H v_k - \left(z_{kj}^s\right)^H S_{kj}\right)^H
$$

radial network

BFM-radial  
\n
$$
s_{j} = \sum_{k,j\sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| a_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{kj} \left( z_{jk}^{*} \right)^{H} S_{kj} \right) - \left| z_{jk}^{*} \right|^{2} \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{kj}^{*} \right)^{H} S_{kj} \right) - \left| z_{kj}^{*} \right|^{2} \ell_{kj}
$$
\n
$$
s_{jk} = \int_{\text{rel}^{+}} \left| a_{kj} \right|^{2} v_{k} - \left( z_{jk}^{*} \right)^{H} S_{jk} = \left( a_{kj}^{H} v_{k} - \left( z_{kj}^{*} \right)^{H} S_{kj} \right)^{H}
$$
\n
$$
s_{jk} = \left| a_{kj}^{H} v_{k} - \left( z_{jk}^{*} \right)^{H} S_{kj} \right|
$$
\n
$$
s_{jk} = \sum_{k,j\sim k} S_{jk} = \left( a_{kj}^{H} v_{k} - \left( z_{kj}^{*} \right)^{H} S_{kj} \right)^{H}
$$
\n
$$
s_{jk} = \sum_{k,j\sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| a_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{*} \right)^{H} S_{jk} \right) - \left| z_{jk}^{*} \right|^{2} \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{jk}^{*} \right)^{H} S_{kj} \right) - \left| z_{kj}^{*} \right|^{2} \ell_{jk}
$$
\n
$$
\left|
$$

BFM-radial  
\n
$$
s_j = \sum_{k,j\sim k} S_{jk}, \quad |S_{jk}|^2 = v_j \ell_{jk}, \quad |S_{kj}|^2 = v_k \ell_k
$$
\n
$$
|a_{jk}|^2 v_j - v_k = 2 \operatorname{Re} \left( a_{jk} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{jk}^* \right|^2 \ell_{jk}
$$
\n
$$
|a_{kj}|^2 v_k - v_j = 2 \operatorname{Re} \left( a_{kj} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^* \right|^2 \ell_{kj}
$$
\n
$$
s_j = \sum_{k,j\sim k} S_{jk} = \left( a_{kj} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^* \right|^2 \ell_{kj}
$$
\n
$$
s_j = \sum_{k,j\sim k} S_{jk} = \left( a_{jk} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right)^{\mathsf{H}}
$$
\n
$$
s_j = \sum_{k,j\sim k} S_{jk} = \left( a_{kj} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right)^{\mathsf{H}}
$$
\n
$$
s_j = \sum_{k,j\sim k} S_{jk}, \quad |S_{jk}|^2 = v_j \ell_{jk}, \quad |S_{kj}|^2 = v_k \ell_{kj}
$$
\n
$$
|a_{jk}|^2 v_j - v_k = 2 \operatorname{Re} \left( a_{jk} \left( z_j^* \right)^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^* \right|^2 \ell_{jk}
$$
\n
$$
|a_{kj}|^2 v_k - v_j = 2 \operatorname{Re} \left( a_{kj} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^* \right|^2 \ell_{kj}
$$
\n
$$
|a_{kj}|^2 v_k - v_j = 2 \operatorname{Re} \left( a_{kj} \left( z_j^* \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^* \right|^2 \ell_{kj}
$$
\n
$$
|a_{kj}|^2 v_k - v_j = 2 \operatorname{Re} \left( a_{kj} \left( z_j^* \right)^{\math
$$

## **Equivalence**

Branch flow models have been most useful for radial networks

- Different variants have different vars and different equations
- Are they equivalent, in what sense?

All BFM variants are equivalent to each other, and to BIM

- BFM-radial: tree topology (cycle condition: linear)
- DistFlow: tree topology with  $y_{jk}^s = y_{kj}^s$  and  $y_{jk}^m = y_{kj}^m = 0$  (cycle condition: vacuous)
- BFM-real: BFM for general topology (cycle condition: nonlinear)
- BFM-complex: bridge to BIM-complex

We next state and prove these equivalence relations

## **Equivalence Solution set**

BIM-complex

$$
s_{j} = \sum_{k:j \sim k} \left( y_{jk}^{s} \right)^{H} \left( |V_{j}|^{2} - V_{j}V_{k}^{H} \right) + \left( y_{jj}^{m} \right)^{H} |V_{j}|^{2}
$$

Solution set

 $V := \{(s, V) \in \mathbb{C}^{2(n+1)} \mid V \text{ satisfies } \text{BIM}\}\$ 

### **Equivalence Solution set**

Branch flow models: solution sets

$$
\tilde{\mathbb{X}} := \{ \tilde{x} : (s, V, I, S) \in \mathbb{C}^{2(N+1)+4M} \mid \tilde{x} \text{ satisfies BFM complex} \}
$$
\n
$$
\mathbb{X}_{\text{meshed}} := \{ x : (s, v, \ell, S) \in \mathbb{R}^{3(N+1)+6M} \mid x \text{ satisfies BFM real} \}
$$
\n
$$
\mathbb{X}_{\text{tree}} := \{ x : (s, v, \ell, S) \in \mathbb{R}^{9N+3} \mid x \text{ satisfies BFM radial} \}
$$
\n
$$
\mathbb{X}_{\text{df}} := \{ x : (s, v, \ell, S) \in \mathbb{R}^{6N+3} \mid x \text{ satisfies BFM radial}, y_{jk}^{s} = y_{kj}^{s}, y_{jk}^{m} = y_{kj}^{m} = 0 \}
$$

<u>Definition</u>: Two sets  $A$  and  $B$  are equivalent  $(A \equiv B)$  if there is a bijection between them

•  $x$  is a power flow solution of  $A$  iff  $g(x)$  is a power flow solution of  $B$ 

## **Equivalence**

#### **Theorem**

Suppose  $G$  is connected

- 1.  $V \equiv \tilde{X} \equiv X_{\text{meshed}}$
- 2. If  $G$  is a tree, then  $\,\mathbb{X}_{\mathsf{meshed}}\equiv\mathbb{X}_{\mathsf{tree}}\,$
- 3. If  $G$  is a tree and  $y_{jk}^s = y_{kj}^s$ ,  $y_{jk}^m = y_{kj}^m = 0$ , then  $\mathbb{X}_{\text{tree}} \equiv \mathbb{X}_{\text{df}}$
# **Equivalence**

Bus injection models and branch flow models are equivalent

• Any result proved in one model holds also in another model

Some results are easier to formulate / prove in one model than the other

- BIM: semidefinite relaxation of OPF (later)
- BFM: some exact relation proofs

Should freely use whichever is more convenient for problem at hand

BFM is particularly suitable for modeling distribution systems

- Tree topology allows efficient computation of power flows (BFS)
- Models and relaxations extend to unbalanced 3 $\phi$  networks
- Seems to be much more numerically stable than BIM for large networks

$$
\mathbf{x}_{\text{tree}} = \frac{\mathbf{E}\mathbf{q}\mathbf{u}\mathbf{v}\mathbf{a}\mathbf{b}\mathbf{c}}{\left| \left| \left| \alpha_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^{*} \right)^{H} S_{jk} \right) - \left| z_{jk}^{*} \right|^{2} \epsilon_{jk}} - \frac{\mathbf{E}\mathbf{q}\mathbf{u}\mathbf{v}\mathbf{a}\mathbf{b}\mathbf{c}\mathbf{b}}{\left| \left| \left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{*} \right)^{H} S_{kj} \right) - \left| z_{kj}^{*} \right|^{2} \epsilon_{jk}} \right| \right|^{2} \epsilon_{kj}
$$
\n
$$
\left| \left| \alpha_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^{*} \right)^{H} S_{kj} \right) - \left| z_{kj}^{*} \right|^{2} \epsilon_{kj}
$$
\n
$$
\left| \alpha_{jk} \right|^{2} v_{j} - \left( z_{jk}^{*} \right)^{H} S_{jk} = \left( \alpha_{kj}^{*} v_{k} - \left( z_{kj}^{*} \right)^{H} S_{kj} \right)^{H}
$$
\n
$$
\left| \alpha_{jk}^{*} v_{j} - \left( z_{jk}^{*} \right)^{H} S_{jk} = \left( \alpha_{kj}^{*} v_{k} - \left( z_{kj}^{*} \right)^{H} S_{kj} \right)^{H}
$$
\n
$$
S_{\text{meshed}}
$$
\n
$$
S_{\text{free}} = \frac{\mathbf{E}\mathbf{q}\mathbf{a}\mathbf{b}\mathbf{b}\mathbf{b}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{c}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{c}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{c}\mathbf{c}\mathbf{c}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{b}\mathbf{c}\mathbf{c}\
$$

#### **Equivalence proof Proof**  $\mathbb{V} \equiv \tilde{\mathbb{X}}$  and  $\mathbb{X}_{\text{tree}} \equiv \mathbb{X}_{\text{df}}$

Straightforward.

$$
\tilde{\chi}
$$
\n
$$
s_j = \sum_{k:j \sim k} S_{jk},
$$
\n
$$
I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k, \quad I_{kj} = \tilde{y}_{kj} V_k - y_{kj}^s V_j
$$
\n
$$
S_{jk} = V_j I_{jk}^H, \quad S_{kj} = V_k I_{kj}^H
$$

$$
s_{j} = \sum_{k:j \sim k} (y_{jk}^{s})^{\mathsf{H}} (|V_{j}|^{2} - V_{j}V_{k}^{\mathsf{H}}) + (y_{jj}^{m})^{\mathsf{H}} |V_{j}|^{2}
$$

$$
s_j = \sum_{k:j \sim k} S_{jk}, \qquad \left| S_{jk} \right|^2 = v_j \ell_{jk}, \qquad \left| S_{kj} \right|^2 = v_k \ell_{kj}
$$
\n
$$
\left| \alpha_{jk} \right|^2 v_j - v_k = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^s \right)^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
\left| \alpha_{kj} \right|^2 v_k - v_j = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^s \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
\left| \alpha_{kj} \right|^2 v_k - v_j = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^s \right)^{\mathsf{H}} S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
\left| v_j - v_k = 2 \operatorname{Re} \left( z_{jk}^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
\left| v_j - v_k = 2 \operatorname{Re} \left( z_{jk}^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
\left| v_j \ell_{jk} = \left| S_{jk} \right|^2
$$

W			
\n $\mathbf{O} \mathbf{U} \mathbf{V} \mathbf{A} \mathbf{I} \mathbf{I$			

 $Fix \tilde{x} := (s, V, I, S) \in \tilde{\mathbb{X}}$ . Define  $v_j := |V_j|^2$ ,  $e_{jk} := |I_{jk}|^2$ ,  $e_{kj} := |I_{kj}|^2$ 

Will show  $x:=(s,v,\ell,S)\in\mathbb{X}$ meshed It suffices to show

**Proof** 

$$
\left| \alpha_{jk} \right|^2 v_j - v_k = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^s \right)^{\mathsf{H}} S_{jk} \right) - \left| z_{jk}^s \right|^2 \mathcal{C}_{jk}
$$
  

$$
\exists \theta \in \mathbb{R}^{N+1} \text{ s.t. } \beta_{jk}(x) = \theta_j - \theta_k, \quad \beta_{kj}(x) = \theta_k - \theta_j
$$

For the 1st equation, write  $V_k = \alpha_{jk} V_j - z_{jk}^s \left( \frac{-\mu}{V} \right)$  and taking square magnitude on both sides. *jk* ( *Sjk*  $V_j$  )

*kj Vj*

 $\tilde{\times}$ 

**Equivalence proof**

\n
$$
\tilde{\mathbb{X}} \equiv \mathbb{X}_{\text{meshed}}
$$

$$
s_{j} = \sum_{k_{j} \sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| a_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\exists \theta \in \mathbb{R}^{N+1} \quad \text{s.t.} \quad \beta_{jk}(x) = \theta_{j} - \theta_{k}, \quad \beta_{kj}(x) = \theta_{k} - \theta_{j}
$$

 $Fix \tilde{x} := (s, V, I, S) \in \tilde{\mathbb{X}}$ . Define  $v_j := |V_j|^2$ ,  $e_{jk} := |I_{jk}|^2$ ,  $e_{kj} := |I_{kj}|$ 

$$
\mathcal{C}_{ki} := |I_{ki}|^2
$$

Will show  $x:=(s,v,\ell,S)\in\mathbb{X}$ meshed For the 2nd equation, we have

$$
V_j V_k^{\mathsf{H}} = \alpha_{jk}^{\mathsf{H}} |V_j|^2 - \left(z_{jk}^s\right)^{\mathsf{H}} S_{jk},
$$

$$
V_{ik} = \left[ \alpha_{kj}^{S} \right]^{H} S_{jk}, \qquad V_{k} V_{j}^{H} = \left[ \alpha_{kj}^{H} |V_{k}|^{2} - \left( z_{kj}^{S} \right)^{H} S_{kj} \right]
$$

**Equivalence proof**

\n
$$
\tilde{\mathbb{X}} \equiv \mathbb{X}_{\text{meshed}}
$$

Fix  $\tilde{x} := (s, V, I, S) \in \tilde{\mathbb{X}}$ . Define

$$
s_{j} = \sum_{k,j\sim k} S_{jk}, \qquad |S_{jk}|^{2} = v_{j} e_{jk}, \qquad |S_{kj}|^{2} = v_{k} e_{kj}
$$
\n
$$
\left| a_{jk} \right|^{2} v_{j} - v_{k} = 2 \text{ Re } \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} e_{jk}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \text{ Re } \left( a_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} e_{kj}
$$
\n
$$
\exists \theta \in \mathbb{R}^{N+1} \text{ s.t. } \beta_{jk}(x) = \theta_{j} - \theta_{k}, \quad \beta_{kj}(x) = \theta_{k} - \theta_{j}
$$

Will show  $x:=(s,v,\ell,S)\in\mathbb{X}$ meshed For the 2nd equation, we have  $v_j := |V_j|^2$ ,  $\ell_{jk} := |I_{jk}|^2$ ,  $\ell_{kj} := |I_{kj}|^2$ 

$$
V_j V_k^{\mathsf{H}} = \alpha_{jk}^{\mathsf{H}} |V_j|^2 - \left(z_{jk}^s\right)^{\mathsf{H}} S_{jk}, \qquad V_k V_j^{\mathsf{H}} = \alpha_{kj}^{\mathsf{H}} |V_k|^2 - \left(z_{kj}^s\right)^{\mathsf{H}} S_{kj}
$$

Recall the nonlinear functions

$$
\beta_{jk}(x) := \angle \left( \alpha_{jk}^H v_j - \left( z_{jk}^s \right)^H S_{jk} \right) = \angle V_j - \angle V_k
$$
\n
$$
\beta_{kj}(x) := \angle \left( \alpha_{kj}^H v_k - \left( z_{jk}^s \right)^H S_{kj} \right) = \angle V_k - \angle V_j
$$

 $\therefore$   $\theta_j := \angle V_j$ 

$W$					
<b>Proof</b>					
$\tilde{x}$	$\tilde{y}$	$\sum S_{jk}$	$ S_{jk} ^2 = v_j \ell_{jk}$	$ S_{jk} ^2 = v_k \ell_{kj}$	
$ q_k ^2 v_j - v_k = 2 \text{Re} \left( a_{jk} \left( z_{jk}^2 \right)^k s_k \right) - \left  z_{jk} \right ^2 \ell_k$					
<b>Proof</b>				$\tilde{X}$	$\equiv$ X <sub>m</sub> eshed
$ a_{ij} ^2 v_k - v_k = 2 \text{Re} \left( a_{ij} \left( z_{ij}^2 \right)^k s_k \right) - \left  z_{ij} \right ^2 \ell_k$					
<b>Proof</b>				$\tilde{X}$	$\equiv$ X <sub>m</sub> eshed
$ a_{ij} ^2 v_k - v_k = 2 \text{Re} \left( a_{ij} \left( z_{ij}^2 \right)^k s_k \right) - \left  z_{ij} \right ^2 \ell_k$					
$ a_{ij} ^2 v_k - v_k = 2 \text{Re} \left( a_{ij} \left( z_{ij}^2 \right)^k s_k \right) - \left  z_{ij} \right ^2 \ell_k$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk}  = v_j t_k^2$					
$ b_{jk} $					

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

W	
\n $\mathbf{O} \mathbf{U} \mathbf{V} \mathbf{A} \mathbf{I} \mathbf{I$	

$$
V_j := \sqrt{v_j} e^{i\theta_j}, \qquad I_{jk} := \sqrt{\ell_{jk}} e^{i(\theta_j - \angle S_{jk})}
$$

Will show  $\tilde{x}:=(s,V,I,S)\in\tilde{\mathbb{X}}$ 

It suffices to show

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

For the 1st equation, we have from  $\left| \right. S_{jk}\right| \;\;=v_{j}\,\ell_{jk}$  and construction of  $(V,I)$ : 2  $=$   $v_j \ell_{jk}^{\prime}$  and construction of  $(V,I)$ 

$$
|S_{jk}| = |V_j I_{jk}^{\mathsf{H}}|, \qquad \angle S_{jk} = \angle V_j - \angle I_{jk}
$$
  
i.e.,  $S_{jk} = V_j I_{jk}^{\mathsf{H}}$ 

**Equivalence proof Proof** ˜ ≡ **meshed** *sj* = ∑*k*:*j*∼*k Sjk*, *Sjk* 2 = *vj ℓjk*, *Skj* 2 = *vk ℓkj αjk* 2 *vj* <sup>−</sup> *vk* <sup>=</sup> <sup>2</sup>Re (*αjk* (*z<sup>s</sup> jk*) *Sjk* ) <sup>−</sup> *<sup>z</sup><sup>s</sup> jk* 2 *ℓjk αkj* 2 *vk* <sup>−</sup> *vj* <sup>=</sup> <sup>2</sup>Re (*αkj* (*z<sup>s</sup> kj*) *Skj* ) <sup>−</sup> *<sup>z</sup><sup>s</sup> kj* 2 *ℓkj* ∃*θ* ∈ ℝ*N*+1 s.t. *βjk*(*x*) = *θ<sup>j</sup>* − *θk*, *βkj* (*x*) = *θ<sup>k</sup>* − *θ<sup>j</sup> sj* = ∑*k*:*j*∼*k Sjk*, *Ijk* = *y*˜*jkVj* − *y<sup>s</sup> jk Vk*, *Ikj* = *y*˜*kj Vk* − *y<sup>s</sup> kj Vj Sjk* = *Vj I jk*, *Skj* = *Vk I kj* ˜ meshed

Conversely, fix  $x := (s, v, \ell, S) \in \mathbb{X}_{\mathsf{meshed}}$ . Construct  $(V, I)$  from  $x$ :

$$
V_j := \sqrt{v_j} e^{i\theta_j}, \qquad I_{jk} := \sqrt{\mathscr{C}_{jk}} e^{i(\theta_j - \angle S_{jk})}
$$

Will show  $\tilde{x}:=(s,V,I,S)\in\tilde{\mathbb{X}}$ 

It suffices to show

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

Note that the 2nd equation is equivalent to (recall  $\tilde{y}^s_{jk} := y^s_{jk} + y^m_{jk}$ ):

$$
z_{jk}^s \left( S_{jk} / V_j \right)^{\mathsf{H}} = \alpha_{jk} V_j - V_k \iff V_j V_k^{\mathsf{H}} = \alpha_{jk}^{\mathsf{H}} v_j - \left( z_{jk}^s \right)^{\mathsf{H}} S_{jk}
$$

We now show that  $\ V_jV_k^{\mathsf{H}}$  and  $\alpha_{jk}^{\mathsf{H}}v_j -\left(z_{jk}^{s}\right)$   $\ S_{jk}$  have equal magnitudes and angles.

<b>Proof</b>			
\n $\tilde{X} = \sum_{k_j \neq k} S_{jk}$ \n	\n $s_j = \sum_{k_j \neq k} S_{jk}$ \n	\n $s_{kj} = \sum_{k_j \neq k} S_{jk}$ \n	\n $s_{kj} = \sum_{k_j \neq k} S_{jk}$ \n
\n $ a_{jk} ^2 v_j - v_k = 2 \text{Re} \left( a_{jk} \left( z_{jk}^* \right)^k s_{jk} \right) - \left  z_{jk}^* \right ^2 \left  e_{jk} \right $ \n	\n $y_j = \sum_{k_j \neq k} S_{jk}$ \n		
\n $ a_{jk} ^2 v_k - v_j = 2 \text{Re} \left( a_{kj} \left( z_{kj}^* \right)^k s_{kj} \right) - \left  z_{jk}^* \right ^2 \left  e_{jk} \right $ \n			
\n $0$ or $\tilde{X} \equiv \sum_{k} \text{Re} \left( \frac{R_{jk}}{k} \right)^k$ \n			
\n $0$ or $\tilde{X} \equiv \sum_{k} \text{Re} \left( \frac{R_{jk}}{k} \right)^k$ \n	\n $0$ or $\tilde{X} \equiv \sum_{k} \left( \frac{R_{jk}}{k} \right)^k$ \n		
\n $0$ or $\tilde{X} \equiv \sum_{k} \text{Re} \left( \frac{R_{jk}}{k} \right)^k$ \n	\n $0$ or $\tilde{X} \equiv \sum_{k} \left( \frac{R_{jk}}{k} \right)^k$ \n		
\n $0$ or $\sum_{k} \sum_{k} \left( \frac{R_{jk}}{k} \right)^k$ \n	\n $0$ or $\sum_{k} \sum_{k} \left( \frac{R_{jk}}{k} \right)^k$ \n		

Will show  $\tilde{x}:=(s,V,I,S)\in\tilde{\mathbb{X}}$ 

It suffices to show

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

 $\mathsf{By \ definition, } \ \beta_{jk}(x) \ := \ \ \angle\Big(\alpha^{\mathsf{H}}_{jk}\,v_j - \left(z^{\mathsf{s}}_{jk}\right) \ \ S_{jk} \ \Big) \ \ = \ \ \theta_j - \theta_k \ \ = \ \ \angle\Big(\,V_jV^{\mathsf{H}}_k\Big)$ 

Example 1.1								
\n $s_j = \sum_{k,j,k} S_{jk}$ \n	\n $ s_k ^2 = v_j e_{jk}$ \n	\n $ s_{kj} ^2 = v_j e_{jk}$ \n	\n $ s_{kj} ^2 = v_k e_{kj}$ \n					
\n $ a_k ^2 v_j - v_k = 2 \text{Re} \left( \alpha_k \left( z_k^* \right)^{11} S_k \right) - \left  z_k^* \right ^2 e_{jk}$ \n	\n $ s_{jk} ^2 e_{jk}$ \n							
\n $ a_k ^2 v_j - v_k = 2 \text{Re} \left( \alpha_k \left( z_k^* \right)^{11} S_k \right) - \left  z_k^* \right ^2 e_{jk}$ \n	\n $ s_{jk} ^2 e_{kj}$ \n							
\n $0.5$ \n	\n $ a_{kj} ^2 v_k - v_j = 2 \text{Re} \left( \alpha_k \left( z_k^* \right)^{11} S_k \right) - \left  z_k^* \right ^2 e_{kj}$ \n	\n $ s_{jk} ^2 e_{kj}$ \n						
\n $0.6$ \n	\n $0.6$ \n	\n $0.6$ \n	\n $0.6$ \n	\n $0.6$ \n	\n $0.6$ \n	\n $0.6$ \n	\n $0.7$ \n	\n $0.8$ \n
\n $0.8$ \n	\n $0.7$ \n	\n $0.8$ \n	\n $0.9$ \n	\n $0.9$ \n	\n $0.9$ \n	\n $0.9$ \n	\n $0.9$ \n	\n $0.$

$$
V_j := \sqrt{v_j} e^{i\theta_j}, \qquad I_{jk} := \sqrt{\mathscr{C}_{jk}} e^{i(\theta_j - \angle S_{jk})}
$$

Will show  $\tilde{x}:=(s,V,I,S)\in\tilde{\mathbb{X}}$ 

It suffices to show

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

For magnitude:

$$
\left| \alpha_{jk}^{H} v_{j} - z_{jk}^{sH} S_{jk} \right|^{2} = \left| \alpha_{jk} \right|^{2} v_{j}^{2} - 2v_{j} \text{Re} \left( \alpha_{jk} z_{jk}^{sH} S_{jk} \right) + \left| z_{jk}^{s} \right|^{2} \left| S_{jk} \right|^{2}
$$
  
=  $v_{j} \left( \left| \alpha_{jk} \right|^{2} v_{j} - 2 \text{Re} \left( \alpha_{jk} z_{jk}^{sH} S_{jk} \right) + \left| z_{jk}^{s} \right|^{2} \mathcal{C}_{jk} \right) = v_{j} v_{k}$ 

<b>Equation 1</b>			
<b>Equation 2</b>			
<b>Equation 3</b>			
$\frac{\sqrt{100}}{100}$			
$\frac{1}{2}$			
$\frac{\sqrt{100}}{100}$			
$\frac{1}{2}$			

$$
S_{jk} = V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k,
$$

This completes the proof of  $\tilde{\mathbb{X}}\equiv\mathbb{X}_{\mathsf{meshed}}$ 

## **Equivalence proof Proof**  $X_{\text{meshed}} \equiv X_{\text{tree}}$

Suppose  $G$  is a tree.

Will show  $x:=(s,v,\ell,S)\in\mathbb{X}_{\mathsf{meshed}}\;\;\Longleftrightarrow\;\;x\in\mathbb{X}_{\mathsf{tree}}$ It suffices to show nonlinear cycle condition becomes linear:

$$
\beta_{jk}(x) := \theta_j - \theta_k = -\beta_{kj}(x)
$$

$$
\iff \alpha_{jk}^H v_j - \left(z_{jk}^s\right)^H S_{jk} = \left(\alpha_{kj}^H v_k - \left(z_{kj}^s\right)^H S_{kj}\right)^H
$$

$$
\chi_{\text{tree}}
$$
\n
$$
s_j = \sum_{k_j \sim k} S_{jk}, \qquad \left| S_{jk} \right|^2 = v_j \ell_{jk}, \qquad \left| S_{kj} \right|^2 = v_k \ell_{kj}
$$
\n
$$
\left| a_{jk} \right|^2 v_j - v_k = 2 \text{Re} \left( a_{jk} \left( z_{jk}^s \right)^H S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^2 v_k - v_j = 2 \text{Re} \left( a_{kj} \left( z_{kj}^s \right)^H S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
a_{jk}^H v_j - \left( z_{jk}^s \right)^H S_{jk} = \left( a_{kj}^H v_k - \left( z_{kj}^s \right)^H S_{kj} \right)^H
$$

radial network  
\n
$$
s_j = \sum_{k,j \sim k} S_{jk}, \qquad |S_{jk}|^2 = v_j \ell_{jk}, \qquad |S_{kj}|^2 = v_k \ell_{kj}
$$
\n
$$
|\alpha_{jk}|^2 v_j - v_k = 2 \operatorname{Re} \left( \alpha_{jk} \left( z_{jk}^s \right)^H S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
|\alpha_{kj}|^2 v_k - v_j = 2 \operatorname{Re} \left( \alpha_{kj} \left( z_{kj}^s \right)^H S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
\exists \theta \in \mathbb{R}^{N+1} \text{ s.t. } \beta_{jk}(x) = \theta_j - \theta_k, \quad \beta_{kj}(x) = \theta_k - \theta_j
$$

*Necessity*: suppose  $x$  satisfies LHS.  $\;\;$  Then angles of RHS satisfy:

$$
\angle \left( \alpha_{jk}^{\mathsf{H}} v_j - z_{jk}^{\mathsf{sH}} S_{jk} \right) = \beta_{jk}(x) = -\beta_{kj}(x) = -\angle \left( \alpha_{kj}^{\mathsf{H}} v_k - z_{kj}^{\mathsf{sH}} S_{kj} \right)
$$

We now show that they have equal magnitudes as well:

$$
\left| \alpha_{jk}^{H} v_j - \left( z_{jk}^{s} \right)^{H} S_{jk} \right|^2 = | \alpha_{jk} |^2 v_j^2 + | z_{jk}^{s} |^2 | S_{jk} |^2 - 2 v_j \text{Re} \left( \alpha_{jk} z_{jk}^{sH} S_{jk} \right) = v_j v_k = \left| \alpha_{kj}^{H} v_k - \left( z_{kj}^{s} \right)^{H} S_{kj} \right|^2
$$

## **Equivalence proof Proof**  $X_{\text{meshed}} \equiv X_{\text{tree}}$

Suppose  $G$  is a tree.

Will show  $x:=(s,v,\ell,S)\in\mathbb{X}_{\mathsf{meshed}}\;\;\Longleftrightarrow\;\;x\in\mathbb{X}_{\mathsf{tree}}$ It suffices to show nonlinear cycle condition becomes linear:

$$
\beta_{jk}(x) := \angle \left( \alpha_{jk}^{H} v_j - z_{jk}^{sH} S_{jk} \right) = \theta_j - \theta_k
$$
\n
$$
\iff \alpha_{jk}^{H} v_j - \left( z_{jk}^{s} \right)^{H} S_{jk} = \left( \alpha_{kj}^{H} v_k - \left( z_{kj}^{s} \right)^{H} S_{kj} \right)^{H}
$$

$$
x_{\text{tree}}
$$
\n
$$
s_j = \sum_{k:j-k} S_{jk}, \qquad \left| S_{jk} \right|^2 = v_j \ell_{jk}, \qquad \left| S_{kj} \right|^2 = v_k \ell_k
$$
\n
$$
\left| a_{jk} \right|^2 v_j - v_k = 2 \text{Re} \left( a_{jk} \left( z_{jk}^s \right)^H S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^2 v_k - v_j = 2 \text{Re} \left( a_{kj} \left( z_{kj}^s \right)^H S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
a_{jk}^H v_j - \left( z_{jk}^s \right)^H S_{jk} = \left( a_{kj}^H v_k - \left( z_{kj}^s \right)^H S_{kj} \right)^H
$$

radial network  
\n
$$
s_j = \sum_{k,j \sim k} S_{jk}, \qquad |S_{jk}|^2 = v_j \ell_{jk}, \qquad |S_{kj}|^2 = v_k \ell_{kj}
$$
\n
$$
|a_{jk}|^2 v_j - v_k = 2 \text{Re} \left( a_{jk} \left( z_{jk}^s \right)^H S_{jk} \right) - \left| z_{jk}^s \right|^2 \ell_{jk}
$$
\n
$$
|a_{kj}|^2 v_k - v_j = 2 \text{Re} \left( a_{kj} \left( z_{kj}^s \right)^H S_{kj} \right) - \left| z_{kj}^s \right|^2 \ell_{kj}
$$
\n
$$
\exists \theta \in \mathbb{R}^{N+1} \text{ s.t. } \beta_{jk}(x) = \theta_j - \theta_k, \quad \beta_{kj}(x) = \theta_k - \theta_j
$$

 $\mathcal S$ *ufficiency*: suppose  $x$  satisfies RHS.

Recall the angle recovery procedure where, since  $G$  is a tree, there is a unique voltage angle (up to  $\theta := C(C^{\mathsf{T}}C)^{-1}\beta(x) + \phi\mathbf{1}$  s.t.  $\beta(x) = C^{\mathsf{T}}\theta$ 

i.e.,  $x$  satisfies the LHS.

This completes the equivalence proof.

# **Outline**

- 1. Radial network
- 2. Equivalence
- 3. Backward forward sweep
	- General BFS
	- Example algorithms
- 4. Linear power flow model

## **Backward forward sweep General formulation**

Efficient solution method for power flow equations

• Special Gauss-Seidel method that is applicable only to radial networks

Partition variables into two groups  $x$  and  $y$ 

• Typically,  $x$  are branch variables (e.g. line currents) and  $y$  are nodal variables (bus voltages)

Design power flow equations as fixed points:  $x = f(x, y)$ ,  $y = g(x, y)$ 

• Choose  $(f, g)$  to have a spatially recursive structure enabled by tree topology

Consists of an outer loop where each outer iteration is implemented by two inner loops

- Outer loop: temporal update over t of  $(x(t), y(t))$  to converge to a fixed point
- Backward sweep at  $t$  : spatial Gauss-Seidel update over nodes  $j$  of  $x_j(t)$ , with  $y(t-1)$  held fixed
- Forward sweep at  $t$  : spatial Gauss-Seidel update over nodes  $j$  of  $y_j(t)$ , with newly computed  $x(t)$  held fixed

Different BFS algorithms differ in choice of variables  $(x, y)$  and design of  $(f, g)$ 

 $\cdot$   $(f, g)$  that is spatially recursive automatically translates into a BFS algorithm

#### **Backward forward sweep Spatially recursive Gauss-Seidel**

At each outer iteration  $t$ , spatial Gauss-Seidel update over  $j$  normally takes the form

$$
x_j(t) := f_j(x_1(t), ..., x_{j-1}(t), x_j(t-1), ..., x_{n_1}(t-1); y(t-1))
$$
  

$$
y_j(t) := g_j(x(t); y_1(t), ..., y_{j-1}(t), y_j(t-1), ..., y_{n_2}(t-1))
$$



# **Example: complex form BFM**

**Assumptions:** radial network and  $z_{jk}^s = z_{kj}^s$ 

- Can use directed graph (with down orientation) and involve line variables only in direction of the lines
- Can uniquely identify a line variable by its from-node or to-node

Then complex form BFM becomes

$$
s_j = \sum_{k:j \sim k} V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k
$$

Given:  $(V_0, s_j, j \in N)$ , find  $(s_0, V_j, j \in N$ ,  $I_{jk}, S_{jk}, j \rightarrow k \in E)$ 

# **Example: complex form BFM**

Complex form BFM

$$
s_j = \sum_{k:j \sim k} V_j I_{jk}^{\mathsf{H}}, \qquad I_{jk} = \tilde{y}_{jk} V_j - y_{jk}^s V_k
$$

Given:  $(V_0, s_j, j \in N)$ , find  $(s_0, V_j, j \in N$ ,  $I_{jk}, S_{jk}, j \rightarrow k \in E)$ 



Design partitioning  $(x, y)$  and corresponding spatially recursive power flow equations  $(f, g)$ in the variables (*s,V,I,S*) <sup>2</sup> <sup>C</sup>2(*N*+1)+4*<sup>M</sup>* (from (5.4)(5.17)):

- $x$  : line currents  $I_{jk}^s$  across impedance  $z_{jk}^s$
- $y$  : nodal voltages  $V_j$
- Given a solution  $(V_j,I^s_{jk})$ , all other quantities (e.g.  $I_{jk},S_{jk}$ ) can be computed
- Can also design BFS that computes sending-end line currents  $I_{jk}$  instead of  $I^s_{jk}$  (Exercise)  $V_{\alpha}$  instead of  $I_{\alpha}^{S}$  (Exercise)  $\mathcal{A}$  is model see in Chapter 6.3 this model serves as a bridge between the bus injection model of Chapter 6.3 this model of Chapter 6.4 thi

#### **Example: complex form BFM Spatially recursive** (*f*, *g*)

Since 
$$
I_{jk}^s := I_{jk} - y_{jk}^m V_j
$$
, KCL at each bus j  
\n
$$
\left(\frac{s_j}{V_j}\right)^H + \left(I_{ij}^s - y_{ji}^m V_j\right) = \sum_{k:j \to k} \left(I_{jk}^s + y_{jk}^m V_j\right)
$$

Spatially recursive power flow equations  $(f,g)$ :

$$
I_{ij}^s = \sum_{k:j \to k} I_{jk}^s - \left( \left( \frac{s_j}{V_j} \right)^H - y_{jj}^m V_j \right) =: f_j \left( x_{\overline{1};}^s y \right)
$$
  

$$
V_j = V_i - z_{ij}^s I_{ij}^s =: g_j \left( x; y_{\overline{1}}^s \right)
$$

where  $i := i(j)$  is unique parent of  $j$  and  $y_{jj}^m := y_{ji}^m + \sum_k y_{jk}^m$ 



#### **Example: complex form BFM BFS**

Spatially recursive power flow equations  $(f,g)$ :

$$
I_{ij}^s = \sum_{k:j \to k} I_{jk}^s - \left( \left( \frac{s_j}{V_j} \right)^H - y_{jj}^m V_j \right) =: f_j(x_{\mathsf{T}_j}^s; y)
$$
  

$$
V_j = V_i - z_{ij}^s I_{ij}^s =: g_j(x; yp_j^s)
$$



This translates automatically to a BFS algorithm with inner loops:

BS: 
$$
x_j(t) := f_j\left(x_{\overline{1}_j}(t); y(t-1)\right)
$$
  
\nFS:  $y_j(t) := g_j\left(x(t); y_{\overline{1}_j}(t)\right)$ 

*i D.* St<br>methods *hethod for weakly meshed distributions*, 3(2):753–762, May 1988. *D*. Shirmohammadi, H. W. Hong, A. Semlyen, and G. X. Luo. A compensation-based power flow<br>method for weakly meshed distribution and transmission networks. *IEEE Transactions on Power*<br>Systems 3(2):753–762 May 1988 **hammadi, H. W. Hong, A. Seml** D. Shirmohammadi, H. W. Hong, A. Semlyen, and G. X. Luo. A compensation-based power flow<br>method for weakly meshed distribution and transmission networks. *IEEE Transactions on Power*<br>Systems 3(2):753–762 May 1988 npensation-based power flow<br>*IEEE Transactions on Power* 

#### **Example: complex form BFM Outer loop** • *y*0(*t*) *y*<sup>0</sup> for *t* = 0*,*1*,...*.

2. while *stopping criterion not met* do

- (a)  $t \leftarrow t + 1$ ;
- (b) *Backward sweep*: for *j starting from leaf nodes and iterating towards bus 0* do

$$
x_j(t) \leftarrow f_j\left(x_{\mathsf{T}_j^{\circ}}(t); y(t-1)\right), \quad j \in \overline{N}
$$

(c) *Forward sweep*: for *j starting from children of bus 0 and iterating towards leaf nodes* do

$$
y_j(t) \leftarrow g_j(x(t); y_{\mathsf{P}_j^{\circ}}(t)), \quad j \in \mathbb{N}
$$

# **Example: complex form BFM**

(b) *Backward sweep*: for *j starting from leaf nodes and iterating towards bus 0* do

$$
I_{ij}^{s}(t) \leftarrow \sum_{k:j\rightarrow k} I_{jk}^{s}(t) - \left( \left( \frac{s_j}{V_j(t-1)} \right)^{\mathsf{H}} - y_{jj}^{m} V_j(t-1) \right), \quad i \rightarrow j \in E
$$

Given all voltages  $V(t-1)$ 

Given all currents  $I_{jk}^s(t)$  in previous layer (in  $T_j^s$ )

Update all currents  $I_{ij}^s(t)$  in present layer (reverse breadth-first search)

#### **Example: complex form BFM** *I i j*(*t*) Â *k*: *j*!*k I jk*(*t*) *Vj*(*t* 1) *ym j jVj*(*t* 1)

(c) *Forward sweep*: for *j starting from children of bus 0 and iterating towards leaf nodes* do

$$
V_j(t) = V_i(t) - z_{ij}^s I_{ij}^s(t), \qquad j \in N
$$

Given all currents  $I^s(t-1)$ Given voltage  $V_i(t)$  at parent of  $j$  (in  $P_j^{\circ}$ ) Update  $V_j(t)$  (breadth-first or depth-first search)

# **Example: DistFlow model**

 $\boldsymbol{\mathsf{Assumptions:}}$  radial network,  $z^s_{jk} = z^s_{kj}$  and  $y^m_{jk} = y^m_{kj} = 0$ 

- Can use directed graph (with up orientation) and involve line variables only in direction of the lines
- Can uniquely identify a line variable by its from-node or to-node

 $\boldsymbol{G}$ iven:  $(V_0, s_j, j \in N)$ , find  $(s_0, v_j, j \in N, \, \ell_{jk}, S_{jk}, j \rightarrow k \in E)$ 

Design partitioning  $(x, y)$  and corresponding spatially recursive power flow equations  $(f, g)$ 

**Line flows:** 
$$
x := (S_{ji(j)}, \ell_{ji(j)}, j \in N) = (S_{jk}, \ell_{jk}, j \to k \in E)
$$

- Nodal voltages:  $y := (v_j, j \in N)$
- Given a solution  $(x, y)$ ,  $s_0$  can be computed

#### **Example: DistFlow model Spatially recursive** (*f*, *g*)

Backward sweep function  $f_j\left(x_{\mathsf{T}^*_j}; y\right)$ :

$$
S_{ji} = s_j + \sum_{k:k \to j} \left( S_{kj} - z_{kj}^s \ell_{kj} \right), \qquad \ell_{ji} = \frac{|S_{ji}|^2}{v_j}
$$

Forward sweep function  $g\left(x, y_{\mathsf{P}_j^*}\right)$ :

$$
v_j = v_i + 2 \operatorname{Re} \left( z_{ji}^s H S_{ji} \right) - |z_{ji}^s|^2 \mathcal{C}_{ji}
$$

This translates automatically to a BFS algorithm with inner loops:

BS: 
$$
x_j(t) := f_j\left(x_{\overline{1}_j^0}(t); y(t-1)\right)
$$
  
\nFS:  $y_j(t) := g_j\left(x(t); y_{\overline{1}_j^0}(t)\right)$ 

# **Outline**

- 1. Radial network
- 2. Equivalence
- 3. Backward forward sweep
- 4. Linear power flow model
	- With shunt admittances
	- Without shunt admittances
	- Linear solution and properties

# **Linear models Advantages**

Linear approximations of BFM have two advantages

- 1. Given nodal injections s, voltages  $v^{\text{lin}}$  and line flows  $S^{\text{lin}}$  can be solved explicitly
- 2. The linear solution  $\left(v^\textsf{lin}, S^\textsf{lin}\right)$  provides bounds on  $(v, S)$  from power flow solutions to nonlinear DistFlow models

Linear approximations are reasonable when line losses  $z_{jk}\mathscr{C}_{jk}$  are small compared with line flows  $S_{jk}$ 

# **With shunt admittances**



 $s_j = \sum S_{jk}$ *k*:*j*∼*k αjk* 2  $v_j - v_k = 2 \text{ Re } \left( \alpha_{jk} \left( z_{jk}^s \right) \right) S_{jk}$ *αkj* 2  $v_k - v_j = 2 \text{ Re } \left( \alpha_{kj} \left( z_{kj}^s \right) \right) S_{kj}$  $\alpha_{jk}^{\text{H}} v_j - \left(z_{jk}^s\right) S_{jk} = \left(a_{kj}^{\text{H}} v_k - \left(z_{kj}^s\right) S_{kj}\right)$ 

BFM-linear

# **With shunt admittances**

 $6N + 2$  linear equations in  $7N + 3$  real variables (*s*, *v*, *S*)

Power flow problem: given  $(v_0, s_j, j \in N)$ , solve for remaining  $5N + 2$  vars  $(s_0, v_j, j \in N)$ 

More equations than unknowns, but they are typically linearly dependent

 $s_j = \sum S_{jk}$ *k*:*j*∼*k αjk* 2  $v_j - v_k = 2 \text{ Re } \left( \alpha_{jk} \left( z_{jk}^s \right) \right) S_{jk}$ *αkj* 2  $v_k - v_j = 2 \text{ Re } \left( \alpha_{kj} \left( z_{kj}^s \right) \right) S_{kj}$  $\alpha_{jk}^{\text{H}} v_j - \left(z_{jk}^s\right) S_{jk} = \left(a_{kj}^{\text{H}} v_k - \left(z_{kj}^s\right) S_{kj}\right)$ 

BFM-linear

# **Example**

#### **2-bus network**

Buses  $j$  and  $k$  connected by a transformer characterized by  $(K, \tilde y^s, \tilde y^m)$  (voltage gain  $K$  may be complex). Let  $\tilde{\alpha} := (1 + \tilde{z}^s \tilde{y}^m)$ .

Linear BFM: 4 linear equations in 6 vars (*s*, *v*)

$$
v_j - v_k / |K|^2 = 2 \operatorname{Re} ((\tilde{z}^s)^H s_j)
$$

$$
|\tilde{\alpha}/K|^2 v_k - v_j = 2 \operatorname{Re} (\tilde{\alpha} (\tilde{z}^s)^H s_k)
$$

$$
v_j - (\tilde{z}^s)^H s_j = (\tilde{\alpha}/|K|^2) v_k - \tilde{z}^s \overline{s}_k
$$

# **Example**

#### **2-bus network**

 $\boldsymbol{\mathsf{Power}}$  flow  $\boldsymbol{\mathsf{problem:}}$  given  $(p_k,q_k,\nu_j)$ , find  $(p_j,q_j,\nu_k)$ 

Assume:  $\tilde{y}^m = 0$  s.t.  $\tilde{\alpha} = 1$ . Then

$$
\begin{bmatrix}\n2\tilde{r} & 2\tilde{x} & -1/|K|^2 \\
0 & 0 & 1/|K|^2 \\
\tilde{r} & \tilde{x} & 1/|K|^2 \\
-\tilde{x} & \tilde{r} & 1/|K|^2\n\end{bmatrix}\n\begin{bmatrix}\np_j \\
q_j \\
v_k\n\end{bmatrix} =\n\begin{bmatrix}\n0 & 0 & 1 \\
2\tilde{r} & 2\tilde{x} & 1 \\
\tilde{r} & \tilde{x} & 1 \\
\tilde{x} & -\tilde{r} & 0\n\end{bmatrix}\n\begin{bmatrix}\np_k \\
q_k \\
v_j\n\end{bmatrix}
$$

Elementary row operation reduces  $A$  to a rank-3 matrix:

$$
\begin{bmatrix}\n(\tilde{r}/\tilde{x})(\tilde{r}^2 + \tilde{x}^2) & 0 & 0 \\
0 & \tilde{r}^2 + \tilde{x}^2 & 0 \\
0 & 0 & 1/|K|^2 \\
0 & 0 & 0\n\end{bmatrix}
$$

# **Without shunt admittances**

$$
s_{j} = \sum_{k,j\sim k} S_{jk}, \qquad \left| S_{jk} \right|^{2} = v_{j} \ell_{jk}, \qquad \left| S_{kj} \right|^{2} = v_{k} \ell_{kj}
$$
\n
$$
\left| a_{jk} \right|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{jk}^{s} \right)^{H} S_{kj} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
\left| a_{kj} \right|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
\left| a_{jk} \left| v_{j} - v_{k} \right| = 2 \operatorname{Re} \left( z_{jk}^{sH} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
\left| v_{j} \ell_{jk} = \left| S_{jk} \right|^{2}
$$
\n
$$
v_{j} \ell_{jk} = \left| S_{jk} \right|^{2}
$$
\n
$$
\ell := 0
$$

$$
\sum_{k:j \to k} S_{jk} = \sum_{i:i \to j} S_{ij} + s_j
$$

$$
v_j - v_k = 2 \operatorname{Re} \left( z_{jk}^{sH} S_{jk} \right)
$$

LinDistFlow

BFM-radial  
\n
$$
s_{j} = \sum_{k,j\sim k} S_{jk}, \quad |S_{jk}|^{2} = v_{j} \ell_{jk}, \quad |S_{kj}|^{2} = v_{k} \ell_{kj}
$$
\n
$$
|a_{jk}|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{jk}
$$
\n
$$
|a_{kj}|^{2} v_{k} - v_{j} = 2 \operatorname{Re} \left( a_{kj} \left( z_{kj}^{s} \right)^{H} S_{kj} \right) - \left| z_{kj}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
s_{jk} = \sum_{k,j\sim k} s_{jk} = \sum_{l: i \rightarrow j} \left( S_{ij} - z_{ij}^{s} \ell_{lj} \right) + s_{j}
$$
\n
$$
v_{j} - v_{k} = 2 \operatorname{Re} \left( z_{jk}^{sH} S_{jk} \right) - \left| z_{jk}^{s} \right|^{2} \ell_{kj}
$$
\n
$$
s_{j} = \sum_{k: j \sim k} S_{jk}
$$
\n
$$
|a_{jk}|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{kj} \right)
$$
\n
$$
s_{j} = \sum_{k: j \sim k} S_{jk}
$$
\n
$$
|a_{jk}|^{2} v_{j} - v_{k} = 2 \operatorname{Re} \left( a_{jk} \left( z_{jk}^{s} \right)^{H} S_{kj} \right)
$$
\n
$$
s_{j} = \sum_{k: j \sim k} s_{jk} = \sum_{l: i \rightarrow j} s_{ij} + s_{j}
$$
\n
$$
s_{j} = \sum_{k: j \sim k} s_{jk} = \sum_{l: i \rightarrow j} s_{lj} + s_{j}
$$
\n
$$
s_{j} = \sum_{l: i \sim j} s_{jl} = \sum_{l: i \sim j} s_{jl} + s_{j}
$$
\n
$$
s_{j} = \sum_{k: j \sim k} s_{jk} = \sum_{l: i \sim j} s_{jl} + s_{j}
$$
\n<math display="block</p>

### **Without shunt admittances LinDistFlow in vector form**

Let

- $C$  : bus-by-line  $(N+1) \times N$  incidence matrix
- $D_r :=$  diag  $(r_l, l \in E) > 0$  : diagonal matrix of line resistances
- $D_x :=$  diag  $(x_l, l \in E) > 0$  : diagonal matrix of line reactances

Then LinDistFlow is:

 $s = CS$ ,  $C^{T}v = 2(D_{r}P + D_{x}Q)$ 

Important features because of tree topology

- $C$  is of rank 1 with null $(C)$  = span(1)
- Reduced  $N \times N$  incidence matrix  $\hat{C}$  is nonsingular
- $\hat{C}^{-1}$  has a simple structure

These features allow explicit linear solutions and structural properties
### **Linear solution**

Let 
$$
C =: \begin{bmatrix} c_0^\mathsf{T} \\ \hat{C} \end{bmatrix}
$$

Then LinDistFlow is:

 $\hat{s} = \hat{C}S$ ,  $s_0 = c_0^{\mathsf{T}}S$  $v_0c_0 + C^{\mathsf{T}}\hat{v} = 2(D_rP + D_xQ)$ 

 $Given$   $(v_0, s_j, j \in N)$ , the remaining variables  $\left(s_0, v_j, j \in N, S_l, l \in E\right)$  can be obtained explicitly

### **Linear solution**

#### **Theorem** [linear solution]

1. Linear solution is:

$$
S = \hat{C}^{-1}\hat{s}, \qquad s_0 = c_0^{\mathsf{T}}\hat{C}^{-1}\hat{s}
$$
  

$$
\hat{v} = v_0 \mathbf{1} + 2(R\hat{p} + X\hat{q})
$$
  
where  $R := \hat{C}^{-\mathsf{T}}D_r\hat{C}^{-1}$  and  $X := \hat{C}^{-\mathsf{T}}D_x\hat{C}^{-1}$ 

2.  $R > 0$  and  $X > 0$  are positive matrices with

$$
R_{jk} = \sum_{l \in P_j \cap P_k} r_l, \qquad X_{jk} = \sum_{l \in P_j \cap P_k} x_l
$$

voltages =  $v_0$  + correction term  $(\hat{p}, \hat{q})$ 

Since entries of  $(R, X)$  are nonnegative, positive injections  $(p, q)$  always increase  $\nu$ 

#### **Analytical properties Special graph orientations**

**Down orientation:** pointing away from bus 0



**Up orientation:** pointing towards bus 0

*i* 0 *j k*  $\overline{S}_{ji}^{\text{lin}} = \sum \overline{S}_{kj}^{\text{lin}} + s_j$  $k:k\rightarrow j$ 

## **Analytical properties**

#### **Corollary**

1. For lines  $(i, j) \in E$ ,  $S_{ij}^{\text{lin}} = \overline{S}_{ji}^{\text{lin}}$ . Moreover  $S_{ij}$ <sup>lin</sup> =  $-\sum$ *k*∈  $s_k$ ,  $i \rightarrow j$  $\overline{S}_{ji}^{\text{lin}} = \sum$ *k*∈  $s_k$ ,  $j \rightarrow i$ line flow  $S_{ij}^{\sf lin}$  to  $j$  supplies all loads  $-s_k$  in subtree line flow  $\overline{S}_{ii}^{\text{lin}}$  from *j* come from all injections  $s_k$  in subtree  $\overline{T}_i$  $S^{\text{III I}}_{ij}$  from  $j$  come from all injections  $s_k$  in subtree  ${\sf T}_j$ 

2. For buses 
$$
j \in \overline{N}
$$
,  $v_j^{\text{lin}} = \overline{v}_j^{\text{lin}} = v_0 + 2 \sum_k \left( R_{jk} p_k + X_{jk} q_k \right)$ 



#### **Analytical properties Nonlinear DistFlow solution**

Linear DistFlow model ignores line losses  $\implies$  simple relation between line flows  $(S_{ij},S_{ji})$  and injections *sk*

Given *s*, nonlinear DistFlow solutions  $(\nu, \ell, S)$  satisfy the recursion in up orientation

$$
S_{ij} = -\sum_{k \in T_j} s_k + \left( z_{ij} \ell_{ij} + \sum_{l \in T_j} z_l \ell_l \right), \qquad v_j = v_0 - \sum_{l \in P_j} \left( 2 \operatorname{Re} \left( z_l^H S_l \right) - \left| z_l \right|^2 \ell_l \right)
$$

and solutions  $(\overline{v}, \mathscr{C}, S)$  satisfy th<mark>e recursion in down orientation</mark>

$$
\overline{S}_{ji} = \sum_{k \in \mathsf{T}_j} s_k - \sum_{l \in \mathsf{T}_j} z_l \overline{\mathcal{E}}_l, \qquad \overline{v}_j = v_0 + \sum_{l \in \mathsf{P}_j} \left( 2 \operatorname{Re} \left( z_l^{\mathsf{H}} \overline{S}_l \right) - |z_l|^2 \overline{\mathcal{E}}_l \right)
$$
\nline losses

## **Bounds on nonlinear solutions**

**Corollary** [bounds on nonlinear solutions]

- 1. For  $i \to j \in E$ ,  $S_{ij} \geq S_{ij}^{\text{lin}}$
- 2. For  $j \to i \in E$ ,  $\overline{S}_{ji} \ge \overline{S}_{ji}^{\text{lin}}$

3. For 
$$
j \in \overline{N}
$$
,  $v_j = \overline{v}_j \le \overline{v}_j^{\text{lin}} = v_j^{\text{lin}}$ 

proving  $\overline{\nu}_j \leq \overline{\nu}_j^{\sf lin}$  is easy; proving directly  $v_j \leq v_j^{\sf lin}$  is not LinDistFlow ignores losses and underestimates required power to supply loads

# **Summary**

- 1. Radial network
	- BFM with and without shunt admittances
	- Nonlinear (quadratic) power flow equations
- 2. Equivalence
	- BFM variants are all equivalent, and equivalent to BIM
- 3. Backward forward sweep
	- Gauss-Seidel method that exploits spatially recursive structure enabled by tree topology
- 4. Linear power flow model
	- Linear BFM with and without shunt admittances
	- Explicit linear solution and bounds on nonlinear solutions
- 5. Application: volt/var control
	- Local and memoryless control can stabilize voltages and implicitly minimizes cost determined by control design