

Power System Analysis

Chapter 6 Example applications

Outline

1. Voltage control
2. Radial network identification

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1. Voltage control
 - Linear DistFlow model
 - Decentralized control: convergence and optimality
2. Radial network identification

volt/var control

Stabilize voltages on distribution grid by adapting reactive power injections

- e.g., at inverters, capacitor banks

Questions we will study

- How to design simple control schemes?
- What is the dynamic behavior of closed-loop system?
- What is the optimality of closed-loop system?

Design and analysis method

- Use LinDistFlow model due to its analytical properties

volt/var control

Network model

At each bus j , there are

- Fixed and given active and reactive load (p_j^0, q_j^0)
- Possibly a DER (e.g. inverter) with fixed p_j (e.g. PV generation) and controllable q_j

Notation: write $s = (p, q) \in \mathbb{R}^{2N}$ and $v \in \mathbb{R}^N$ at non-reference buses, instead of (\hat{s}, \hat{v})

From linear solution theorem:

$$v = v_0 \mathbf{1} + 2 (R(p - p^0) + X(q - q^0))$$

Or

$$v(q) = 2Xq + \tilde{v}$$

where $\tilde{v} := v_0 \mathbf{1} + 2R(p - p^0) - 2Xq^0$ independent of the control q

volt/var control

Inverter model

At each bus j , the reactive power q_j is constrained to stay in the intersection of

- Capacity limit $\{q_j : p_j^2 + q_j^2 \leq \sigma^2\}$ which depends on p_j (e.g. PV generation), and
- Power factor limit $-\phi_j \leq \tan^{-1}(q_j/p_j) \leq \phi_j$

Hence q_j must lie in

$$U_j := U_j(p_j) \left\{ q_j : \underline{q}_j \leq q_j \leq \bar{q}_j \right\}$$

where $\bar{q}_j := \min \left\{ p_j \tan \phi_j, \sqrt{\sigma^2 - p_j^2} \right\}$ and $\underline{q}_j := \max \left\{ -p_j \tan \phi_j, -\sqrt{\sigma^2 - p_j^2} \right\}$

volt/var control

Local memoryless control

Let v^{ref} = given vector of reference voltages at buses $j > 0$

Control goal: design $q \in U$ to drive voltages towards v^{ref}

- Local control: $q_j(t + 1)$ depends only on $v_j(t)$, not voltages $v_k(t)$ at buses $k \neq j$
- Memoryless control: $q_j(t + 1)$ depends only on $v_j(t)$, not on $(v_j(s), s < t)$

Restrict control law $u_j : \mathbb{R} \rightarrow \mathbb{R}$ to depend on voltage error $v_j(t) - v_j^{\text{ref}}$

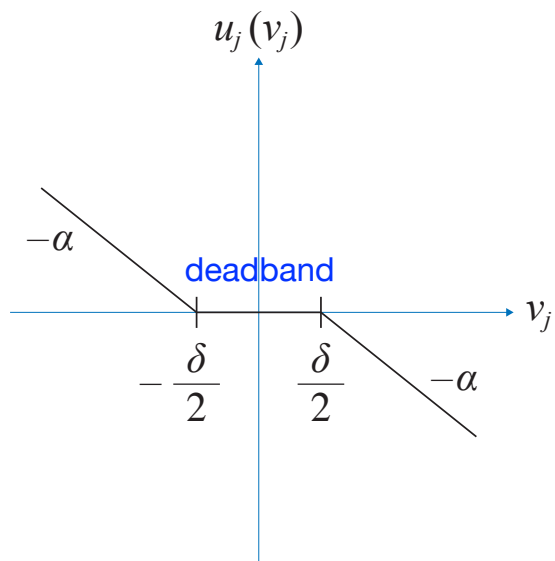
$$q_j(t + 1) = \left[u_j \left(v_j(t) - v_j^{\text{ref}} \right) \right]_{U_j}, \quad j = 1, \dots, N$$

i.e. we are to design u_j that map voltage errors $v_j(t) - v_j^{\text{ref}}$ to reactive power settings $q_j(t + 1)$

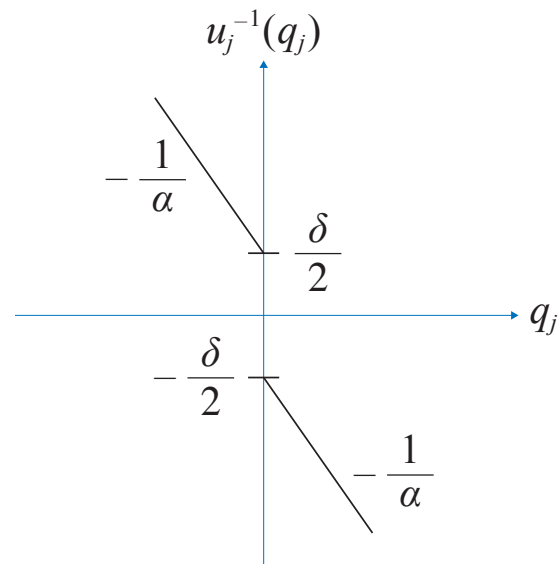
volt/var control

Local memoryless control

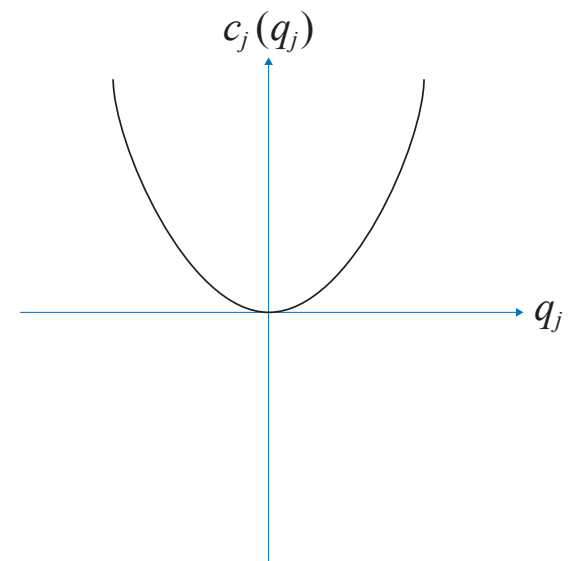
Example:



(a) Piecewise linear control $u_j(v_j)$

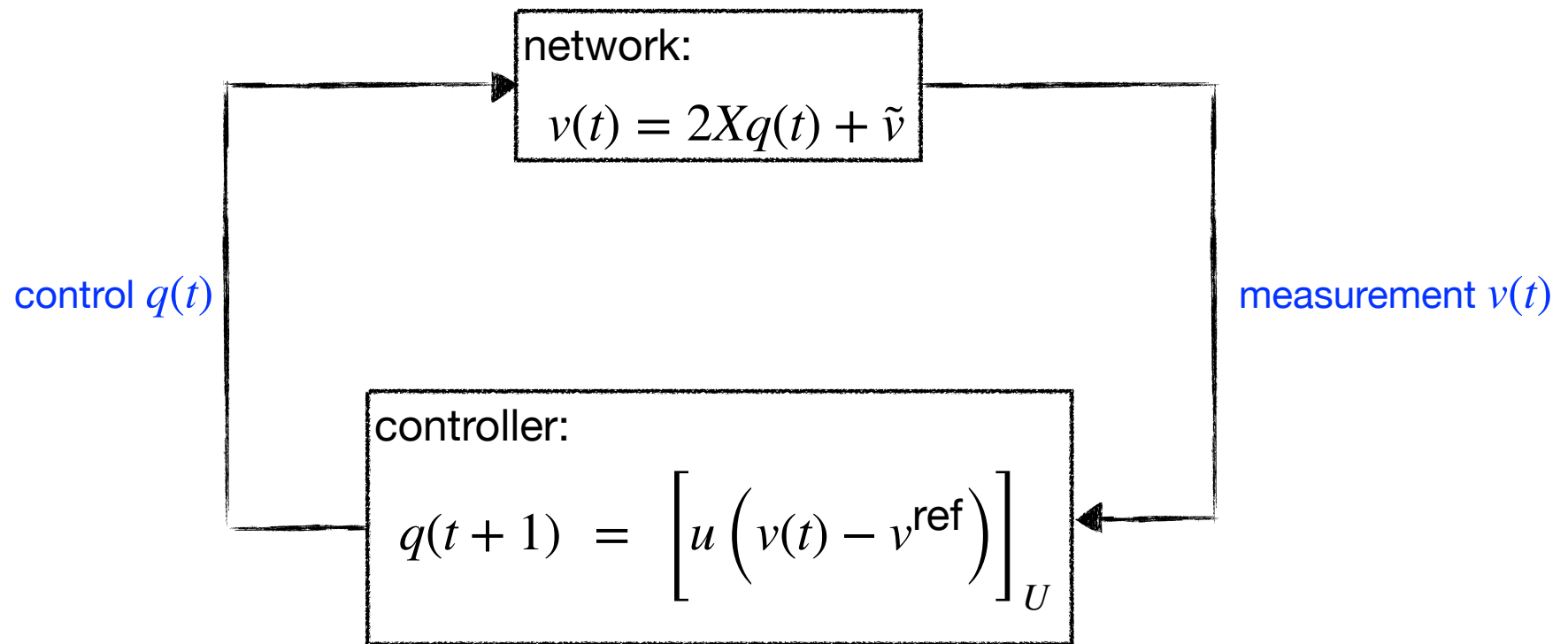


(b) Inverse $u_j^{-1}(q_j)$



(c) Implied cost $c_j(q_j)$

Closed-loop system



Closed-loop system

Closed-loop system is discrete-time dynamical system:

$$q(t+1) = \left[u \left(v(q(t)) - v_j^{\text{ref}} \right) \right]_U$$

- $v(q) := 2Xq + \tilde{v}$: maps linearly reactive power control q to network voltage
- $u \left(v - v^{\text{ref}} \right)$: maps voltage error to potential control action
- $[u]_U$: projects potential control action to its feasibility region U

Questions:

- Stability: will $(q(t), v(t))$ converge to an equilibrium point (q^*, v^*) ?
- Optimality: is the equilibrium point (q^*, v^*) optimal, in what sense?

Closed-loop system

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$$q(t+1) = \left[u \left(v(q(t)) - v_j^{\text{ref}} \right) \right]_U$$

where $v(q) := 2Xq + \tilde{v}$

Definition:

q^* is an **equilibrium point** if it is a fixed point, i.e., $q^* = \left[u \left(v(q^*) - v_j^{\text{ref}} \right) \right]_U$

Assumptions:

1. u_j are differentiable; $\exists \alpha_j$ s.t. $\left| u_j'(v_j) \right| \leq \alpha_j$

$$A := \text{diag} \left(\alpha_j, j \in N \right)$$

2. u_j are strictly decreasing

Convergence

Theorem [Convergence]

Suppose Assumption 1 holds. If largest singular value $\sigma_{\max}(AX) < 1/2$ then

1. \exists unique equilibrium point $q^* \in U$
2. $q(t)$ converges to q^* geometrically, i.e.,

$$\|q(t) - q^*\| \leq \beta^t \|q(0) - q^*\| \rightarrow 0$$

for some $\beta \in [0,1)$

$$A := \text{diag}(\alpha_j, j \in N)$$

Optimality

Theorem [Optimality]

Suppose Assumptions 1 and 2 hold. The **unique equilibrium point** q^* of the dynamical system is the **unique minimizer** of

$$\min_{q \in U} \sum_j c_j(q_j) + q^\top X q + q^\top (\tilde{v} - v^{\text{ref}})$$

where $c_j(q_j) := - \int_0^{q_j} u_j^{-1}(\hat{q}_j) d\hat{q}_j$

Closed-loop behavior

Questions:

- Stability: will $(q(t), v(t))$ converge to an equilibrium point (q^*, v^*) ?
- Optimality: is the equilibrium point (q^*, v^*) optimal, in what sense?

Answer: under assumptions 1 and 2

- $(q(t), v(t))$ converges geometrically to a unique equilibrium point (q^*, v^*)
- The unique equilibrium point (q^*, v^*) minimizes a cost function determined by control law u_j

Reverse engineering: by choosing a control function u_j , we implicitly choose a cost function $c_j(q_j)$ that the closed-loop equilibrium optimizes

Closed-loop behavior

Questions:

- Stability: will $(q(t), v(t))$ converge to an equilibrium point (q^*, v^*) ?
- Optimality: is the equilibrium point (q^*, v^*) optimal, in what sense?

Answer: under assumptions 1 and 2

- $(q(t), v(t))$ converges geometrically to a unique equilibrium point (q^*, v^*)
- The unique equilibrium point (q^*, v^*) minimizes a cost function determined by control law u_j

Forward engineering: Choose a cost function $c_j(q_j)$ and derive control functions u_j as distributed algorithm to solve the optimization problem

Convergence proof

Sketch

Mean value theorem $\implies u_j(v_j) - u(\hat{v}_j) = u'_j(w)(u - \hat{u})$ where $w := \lambda u + (1 - \lambda)\hat{u}$ for some $\lambda \in [0,1]$

Assumption 1 and MVT

Hence

$$\|u(v) - u(\hat{v})\|_2^2 = \sum_j |u_j(v_j) - u_j(\hat{v}_j)|^2 \leq \sum_j |\alpha_j(v_j - \hat{v}_j)|^2 = \|A(v - \hat{v})\|_2^2$$

Therefore

$$\left\| u\left(v(q) - v^{\text{ref}}\right) - u\left(v(\hat{q}) - v^{\text{ref}}\right) \right\|_2 \leq \|Av(q) - Av(\hat{q})\|_2$$

Convergence proof

Sketch

Vector-function mean value theorem: if $f: \mathbb{R}^n \rightarrow \mathbb{R}^n$ is continuously differentiable then

$$\|f(y) - f(x)\| \leq \left\| \frac{\partial f}{\partial x}(z) \right\| \|y - x\|$$

for any induced matrix norm $\|\cdot\|$ where $z := \mu x + (1 - \mu)y$ for some $\mu \in [0,1]$

Hence

$$\|Av(q) - Av(\hat{q})\|_2 \leq \left\| \frac{\partial Av}{\partial q} \right\|_2 \|q - \hat{q}\|_2 \leq \|2AX\|_2 \|q - \hat{q}\|_2$$

because $\frac{\partial Av}{\partial q}(q) = A \frac{\partial v}{\partial q}(q) = 2AX$

Convergence proof

Sketch

Therefore

$$\left\| u \left(v(q) - v^{\text{ref}} \right) - u \left(v(\hat{q}) - v^{\text{ref}} \right) \right\|_2 \leq \|2AX\|_2 \|q - \hat{q}\|_2$$

Since induced matrix norm $\|AX\|_2 = \sigma_{\max}(AX)$, if $\beta = 2\sigma_{\max}(AX) < 1$ then

$$\left\| u \left(v(q) - v^{\text{ref}} \right) - u \left(v(\hat{q}) - v^{\text{ref}} \right) \right\|_2 \leq \beta \|q - \hat{q}\|_2$$

i.e. $u(q)$ is a contraction mapping.

Since projection $[u]_U$ is non-expansive, i.e., $\|[u]_U - [\hat{u}]_U\|_2 \leq \|u - \hat{u}\|_2$, the mapping

$\left[u \left(v(q) - v^{\text{ref}} \right) \right]_U$ is a contraction mapping in q

Convergence proof

Sketch

Contraction theorem implies, for the dynamical system

$$q(t+1) = \left[u \left(v(q(t)) - v_j^{\text{ref}} \right) \right]_U$$

that

- \exists unique fixed point q^*
- $q(t)$ converges to q^* geometrically

Optimality

Theorem [Optimality]

Suppose Assumptions 1 and 2 hold. The **unique equilibrium point** q^* of the dynamical system is the **unique minimizer** of

$$\min_{q \in U} \sum_j c_j(q_j) + q^\top X q + q^\top (\tilde{v} - v^{\text{ref}})$$

where $c_j(q_j) := - \int_0^{q_j} u_j^{-1}(\hat{q}_j) d\hat{q}_j$

Optimality proof

Sketch

Assumption 1 implies that there is a unique equilibrium pt q^*

Let $C(q) := \sum_j c_j(q_j) + q^\top Xq + q^\top \Delta \tilde{v}$ where $\Delta \tilde{v} := \tilde{v} - v^{\text{ref}}$

Assumption 2 and $X \succ 0$ imply that $C(q)$ is strictly convex and hence, if an optimal q^* exists, it is unique

It thus suffices to show that q^* is the unique equilibrium pt if and only if q^* is the unique minimizer

We will show this in 3 steps:

1. Obtain optimality condition (necessary and sufficient because of convexity)

2. Relate $[\nabla C(q^*)]_j$ to $u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right)$ and q^*

3. Conclude optimality condition is equivalent to $q^* = \left[u \left(v(q^*) - v^{\text{ref}} \right) \right]_U$

Optimality proof

Sketch

Step 1: By convexity, $q^* \in U$ is optimal iff

$$(\nabla C(q^*))^\top (q - q^*) \geq 0 \quad \forall q \in U$$

This is equivalent to

$$q_j^* \in (\underline{q}_j, \bar{q}_j) \quad \implies \quad [\nabla C(q^*)]_j = 0$$

$$q_j^* = \underline{q}_j \quad \longleftarrow \quad [\nabla C(q^*)]_j > 0$$

$$q_j^* = \bar{q}_j \quad \longleftarrow \quad [\nabla C(q^*)]_j < 0$$

Optimality proof

Sketch

Step 2: Evaluate

$$\nabla C(q^*) = \nabla c(q^*) + 2Xq^* + \Delta\tilde{v} = \nabla c(q^*) + \left(v(q^*) - v^{\text{ref}} \right)$$

where $\nabla c(q^*) = (c'_j(q_j^*)) = -u_j^{-1}(q_j^*), i \in N$

Hence $[\nabla C(q^*)]_j = -u_j^{-1}(q_j^*) + \left(v_j(q_j^*) - v_j^{\text{ref}} \right)$

Since u_j is strictly decreasing (Assumption 2), we have

$$[\nabla C(q^*)]_j = 0 \iff u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) = q_j^*$$

$$[\nabla C(q^*)]_j > 0 \iff u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) < q_j^*$$

$$[\nabla C(q^*)]_j < 0 \iff u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) > q_j^*$$

Optimality proof

Sketch

Step 3: Use $[\nabla C(q^*)]_j$ to combine the conditions in Steps 1 and 2 into:

$$q_j^* \in (\underline{q}_j, \bar{q}_j) \quad \Longrightarrow \quad [\nabla C(q^*)]_j = 0 \quad \Longleftrightarrow \quad u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) = q_j^*$$

$$q_j^* = \underline{q}_j \quad \Longleftarrow \quad [\nabla C(q^*)]_j > 0 \quad \Longleftrightarrow \quad u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) < \underline{q}_j$$

$$q_j^* = \bar{q}_j \quad \Longleftarrow \quad [\nabla C(q^*)]_j < 0 \quad \Longleftrightarrow \quad u_j \left(v_j(q_j^*) - v_j^{\text{ref}} \right) > \bar{q}_j$$

But this is equivalent to:

$$q^* = \left[u \left(v(q^*) - v^{\text{ref}} \right) \right]_U$$

i.e. q^* is the unique equilibrium point

Therefore q^* is the unique equilibrium pt if and only if q^* is the unique minimizer

Outline

1. Voltage control
2. Radial network identification
 - Linearized polar-form AC model
 - Covariances of voltage magnitudes

Recall: radial networks

When $y_{jk}^s = y_{kj}^s$ and $y_{jk}^m = y_{kj}^m = 0$

Theorem 10

Suppose G is connected, Y is complex symmetric ($y_{jk}^s = y_{kj}^s$) and $y_{jk}^m = y_{kj}^m = 0$.

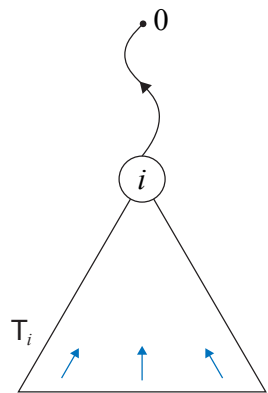
1. Reduced incidence matrix \hat{C} is nonsingular

$$[\hat{C}^{-1}]_{lj} = \begin{cases} -1 & l \in P_j \\ 1 & -l \in P_j \\ 0 & \text{otherwise} \end{cases}$$

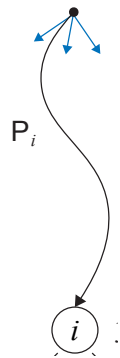
2. Reduced admittance matrix \hat{Y} is nonsingular, and

$$\hat{Z} := \hat{Y}^{-1} = \hat{C}^{-T} D_z^s \hat{C}^{-1}$$

$$\hat{Z}_{jk} = \sum_{l \in P_j \cap P_k} z_l^s$$



T_i : subtree rooted at bus i



T_i : unique path from 0 to i

Apply this result to topology identification problem

Topology identification

1. Distribution grid typically consists of a meshed network with sectionalizing and tie switches on some lines
2. At any time switch are configured s.t. operational network is a spanning tree (substation at its root)
3. System operator knows the meshed network, but may not always know accurately switch status and hence operational network

Goal: Identify operational radial network from measurements of voltage magnitudes

Linearized power flow model

Linearization of polar form

Assumptions: For all $(j, k) \in E$

1. $y_{jk}^s = y_{kj}^s = g_{jk}^s + ib_{jk}^s$; $y_{jk}^m = y_{kj}^m = 0$
2. $g_{jk}^s > 0$ and $b_{jk}^s < 0$

Consider **flat voltage profile**: $V_j^{\text{flat}} = \mu e^{i\theta} \implies (p^{\text{flat}}, q^{\text{flat}}) = (0,0)$

- All voltages have same magnitude (e.g. $\mu = 1$ pu) and angle

Let

- $(|\hat{V}|, \hat{\theta})$: perturbation variable around V^{flat} at non-reference buses
- (\hat{p}, \hat{q}) : perturbation variable around $(p^{\text{flat}}, q^{\text{flat}}) = (0,0)$ at non-reference buses

Linearized power flow model

Linearization of polar form

Polar form power flow model

$$p_j = \sum_{k:k\sim j} (g_{jk}^s + g_{jk}^m) |V_j|^2 - \sum_{k:k\sim j} |V_j| |V_k| (g_{jk}^s \cos \theta_{jk} + b_{jk}^s \sin \theta_{jk})$$

$$q_j = - \sum_{k:k\sim j} (b_{jk}^s + b_{jk}^m) |V_j|^2 - \sum_{k:k\sim j} |V_j| |V_k| (g_{jk}^s \sin \theta_{jk} - b_{jk}^s \cos \theta_{jk})$$

Linearized power flow model

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$$q_j = - \sum_{k:k\sim j} (b_{jk}^s + b_{jk}^m) |V_j|^2 - \sum_{k:k\sim j} |V_j| |V_k| (g_{jk}^s \sin \theta_{jk} - b_{jk}^s \cos \theta_{jk})$$

Linearize around $(V^{\text{flat}}, p^{\text{flat}}, q^{\text{flat}})$ yields a linear model from $|\hat{V}|$ to (\hat{p}, \hat{q}) at non-reference buses:

$$|\hat{V}| = \hat{R}\hat{p} + \hat{X}\hat{q} + \hat{v}_0$$

where

$$\hat{R} := \hat{C}^{-T} D_1 \hat{C}^{-1} > 0, \quad \hat{X} := -\hat{C}^{-T} D_2 \hat{C}^{-1} > 0$$

\hat{C} is reduced incidence matrix and

$$D_g := \text{diag}(g_l^s, l \in E) > 0, \quad D_b := \text{diag}(b_l^s, l \in E) < 0$$

$$D_1 := (D_g + D_b D_g^{-1} D_b)^{-1} > 0, \quad D_2 := (D_b + D_g D_b^{-1} D_g)^{-1} < 0$$

Covariance of voltages and powers

Suppose injections (p, q) vary randomly and induce random fluctuations in $|\hat{V}|$

Define covariance and cross-covariance matrices

$$\Sigma_v := E[|\hat{V}| - E(|\hat{V}|)][(|V| - E(|V|))]^\top$$

$$\Sigma_p := E[\hat{p} - E\hat{p}][\hat{p} - E\hat{p}]^\top,$$

$$\Sigma_q := E[\hat{q} - E\hat{q}][\hat{q} - E\hat{q}]^\top$$

$$\Sigma_{pq} := E[\hat{p} - E\hat{p}][\hat{q} - E\hat{q}]^\top,$$

$$\Sigma_{qp} := E[\hat{q} - E\hat{q}][\hat{p} - E\hat{p}]^\top$$

Then

$$\Sigma_v = \hat{R}\Sigma_p\hat{R}^\top + \hat{X}\Sigma_q\hat{X}^\top + \hat{R}\Sigma_{pq}\hat{X}^\top + \hat{X}\Sigma_{qp}\hat{R}^\top$$

Covariance of voltages and powers

Assumptions: power injections at same bus are positively correlated, those at different buses are uncorrelated

3. For all $j \in N$: $\Sigma_p[j,j] > 0$, $\Sigma_q[j,j] > 0$, $\Sigma_{pq}[j,j] = \Sigma_{qp}[j,j] > 0$; $y_{jk}^m = y_{kj}^m = 0$

4. For all $j \neq k$: $\Sigma_p[j,k] = \Sigma_q[j,k] = \Sigma_{pq}[j,k] = \Sigma_{qp}[j,k] = 0$

Covariance of voltages and powers

Assumptions: power injections at same bus are positively correlated, those at different buses are uncorrelated

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4. For all $j \neq k$: $\Sigma_p[j,k] = \Sigma_q[j,k] = \Sigma_{pq}[j,k] = \Sigma_{qp}[j,k] = 0$

Theorem

Under assumptions 1-4:

1. If a non-reference bus $j \in N$ is a descendant of bus i , then $\text{var}(|V_j|) > \text{var}(|V_i|)$

2. If bus i is a parent of bus j then the variance of $|V_i| - |V_j|$ is given by:

$$E\left(\left(|V_i| - |V_j|\right) - E\left(|V_i| - |V_j|\right)\right)^2 = \sum_{k \in T_j} \left(r_{ij}^2 \text{var}(p_k) + x_{ij}^2 \text{var}(q_k) + 2r_{ij}x_{ij} \text{cov}(p_k, q_k) \right)$$

Covariance of voltages and powers

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$$E\left(\left(|V_i| - |V_j| - E(|V_i| - |V_j|)\right)^2\right) = \sum_{k \in T_j} \left(r_{ij}^2 \text{var}(p_k) + x_{ij}^2 \text{var}(q_k) + 2r_{ij}x_{ij} \text{cov}(p_k, q_k) \right)$$

Implications

Property 1 identifies a leaf node j as one with $\max \text{var}(|V_j|)$

Property 2 identifies j 's parent i as one that most closely satisfies the formula

Algorithm

1. Identify a leaf node j among unidentified nodes.
2. Identify j 's parent.
3. Remove j from set of unidentified nodes and goto 1

Covariance of voltages and powers

Proof: part 1

Theorem 10 implies

$$\hat{R}_{jk} = \sum_{l \in P_j \cap P_k} r_l > 0, \quad \hat{X}_{jk} = \sum_{l \in P_j \cap P_k} x_l > 0$$

Hence

$$\hat{R}_{jk} = \hat{R}_{ik} + r_{ij}, \quad \hat{R}_{ik} = \sum_{l \in P_i} r_l, \quad \text{if } k \in T_j$$

$$\hat{R}_{ik} = \hat{R}_{jk}, \quad \text{if } k \notin T_j$$

Use these to evaluate the diagonal entries of $\text{var}(|V_j|) - \text{var}(|V_i|) = \Sigma_v[j, j] - \Sigma_v[i, i]$, for each of the four terms in

$$\Sigma_v = \hat{R}\Sigma_p\hat{R}^T + \hat{X}\Sigma_q\hat{X}^T + \hat{R}\Sigma_{pq}\hat{X}^T + \hat{X}\Sigma_{qp}\hat{R}^T$$

Covariance of voltages and powers

Due to covariances Σ_p, Σ_q :

$$\left(\hat{R}\Sigma_p\hat{R}^T\right)[j,j] - \left(\hat{R}\Sigma_p\hat{R}^T\right)[i,i] = \sum_{k \in T_j} \Sigma_p[k,k] \left(2 \sum_{l \in P_i} r_l + r_{ij}\right) r_{ij} > 0$$

similarly: $\left(\hat{X}\Sigma_q\hat{X}^T\right)[j,j] > \left(\hat{X}\Sigma_q\hat{X}^T\right)[i,i]$

Due to cross-covariances Σ_{pq}, Σ_{qp} :

$$\left(\hat{R}\Sigma_{pq}\hat{X}^T\right)[j,j] - \left(\hat{R}\Sigma_{pq}\hat{X}^T\right)[i,i] = \sum_k \Sigma_{pq}[k,k] \left(\hat{R}_{jk}\hat{X}_{jk} - \hat{R}_{ik}\hat{X}_{ik}\right) > 0$$

similarly: $\left(\hat{X}\Sigma_{qp}\hat{R}^T\right)[j,j] > \left(\hat{X}\Sigma_{qp}\hat{R}^T\right)[i,i]$

yielding: $\Sigma_v[j,j] > \Sigma_v[i,i]$

Covariance of voltages and powers

Proof: part 2

If bus i is a parent of bus j , then variance of $|V_i| - |V_j|$ is:

$$E \left((|V_i| - E|V_j|) - (|V_i|) - |V_j| \right)^2 = \Sigma_v[i, i] + \Sigma_v[j, j] - 2\Sigma_v[i, j]$$

Again use

$$\hat{R}_{jk} = \hat{R}_{ik} + r_{ij}, \quad \hat{R}_{ik} = \sum_{l \in P_i} r_l, \quad \text{if } k \in T_j$$

$$\hat{R}_{ik} = \hat{R}_{jk}, \quad \text{if } k \notin T_j$$

to show that the first term of

$$\Sigma_v = \hat{R}\Sigma_p\hat{R}^T + \hat{X}\Sigma_q\hat{X}^T + \hat{R}\Sigma_{pq}\hat{X}^T + \hat{X}\Sigma_{qp}\hat{R}^T$$

yields a simple expression:

$$\sigma_1 := \left(\hat{R}\Sigma_p\hat{R}^T \right)[i, i] + \left(\hat{R}\Sigma_p\hat{R}^T \right)[j, j] - 2 \left(\hat{R}\Sigma_p\hat{R}^T \right)[i, j] = r_{ij}^2 \sum_{k \in T_j} \Sigma_p[k, k]$$

Covariance of voltages and powers

Similarly, the other terms of

$$\Sigma_v = \hat{R}\Sigma_p\hat{R}^\top + \hat{X}\Sigma_q\hat{X}^\top + \hat{R}\Sigma_{pq}\hat{X}^\top + \hat{X}\Sigma_{qp}\hat{R}^\top$$

yield

$$\sigma_1 := \left(\hat{R}\Sigma_p\hat{R}^\top\right)[i, i] + \left(\hat{R}\Sigma_p\hat{R}^\top\right)[j, j] - 2\left(\hat{R}\Sigma_p\hat{R}^\top\right)[i, j] = r_{ij}^2 \sum_{k \in \bar{T}_j} \Sigma_p[k, k]$$

$$\sigma_2 := \left(\hat{X}\Sigma_q\hat{X}^\top\right)[i, i] + \left(\hat{X}\Sigma_q\hat{X}^\top\right)[j, j] - 2\left(\hat{X}\Sigma_q\hat{X}^\top\right)[i, j] = x_{ij}^2 \sum_{k \in \bar{T}_j} \Sigma_q[k, k]$$

$$\sigma_3 := \left(\hat{R}\Sigma_{pq}\hat{X}^\top\right)[i, i] + \left(\hat{R}\Sigma_{pq}\hat{X}^\top\right)[j, j] - 2\left(\hat{R}\Sigma_{pq}\hat{X}^\top\right)[i, j] = r_{ij}x_{ij} \sum_{k \in \bar{T}_j} \Sigma_{pq}[k, k]$$

$$\sigma_4 := \left(\hat{X}\Sigma_{qp}\hat{R}^\top\right)[i, i] + \left(\hat{X}\Sigma_{qp}\hat{R}^\top\right)[j, j] - 2\left(\hat{X}\Sigma_{qp}\hat{R}^\top\right)[i, j] = r_{ij}x_{ij} \sum_{k \in \bar{T}_j} \Sigma_{qp}[k, k]$$

Covariance of voltages and powers

Summing:

$$\Sigma_v[i, i] - \Sigma_v[i, j] = \sum_{k=1}^4 \sigma_k = \sum_{k \in \mathbb{T}_j} \left(r_{ij}^2 \Sigma_p[k, k] + x_{ij}^2 \Sigma_q[k, k] + 2r_{ij}x_{ij} \Sigma_{pq}[k, k] \right)$$